
Turbulence

Bjarne Husted, Dr. Ing.

Associate Professor

Department of Fire Safety Engineering

bjarne.husted@brand.lth.se

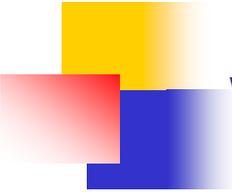
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UNIVERSITY

Fire in wind mill, Denmark, 4. august 2017

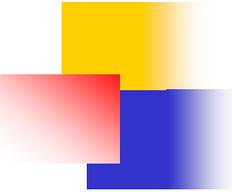




Purpose of lecture

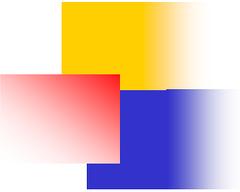
Why is the understanding of turbulence important

- Turbulence is responsible in fires
 - Rate for combustion (mixing) $Da = \frac{\text{flow time scale}}{\text{chemical time scale}}$
 - Entrainment in fire plumes
 - Flow around obstacles
- Explosion
 - Faster mixing, video <https://youtu.be/PdfY3EDrGrQ>
 - Deflagration > Detonation



Overview

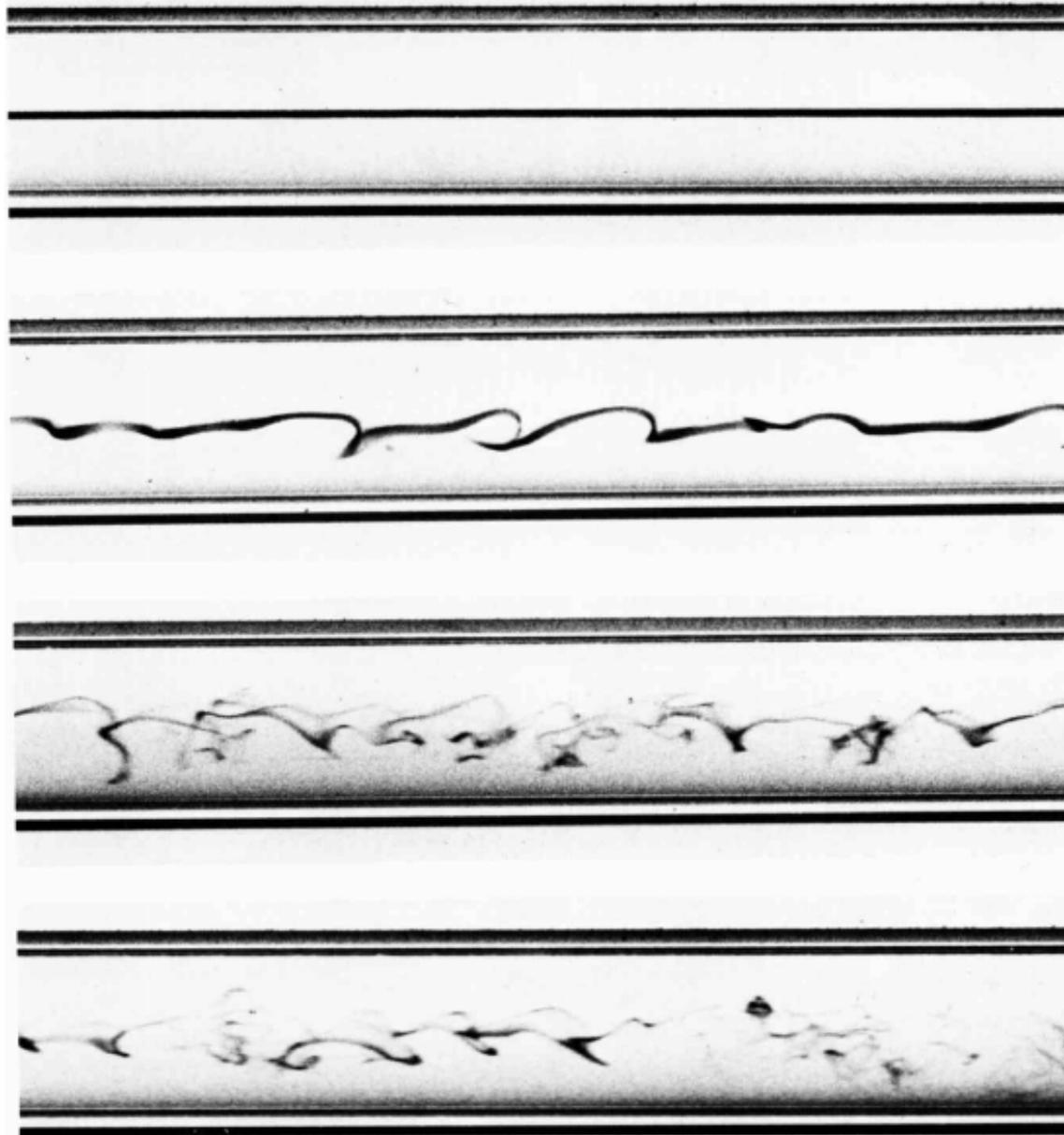
- Laminar and turbulent flow
- What is turbulence
- Reynolds number
- Transition from laminar to turbulent flow
- Treatment of turbulence in CFD codes
 - RANS
 - LES
 - DNS



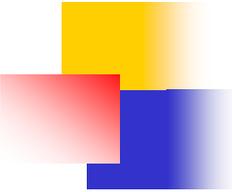
Laminar and turbulent flow

- Most flow of interest are turbulent
 - Flow in pipes
 - Mixing process (eg. pharmaceutical industry)
 - Fires
- Transition between laminar and turbulent flow can be determined by the Reynolds number. For a pipe flow the transition happens between 2000 – 3000. Flow over a plate: $Re_x \approx 5 \cdot 10^5$

Repetition of Osborne Reynolds dye experiment from 1883



Source: Van Dyke, *An Album of Fluid Motion*, Stanford, 1982 (p. 61)



Find the Reynolds number

- Definition

$$\text{Re} = \frac{\rho \cdot U \cdot D_h}{\mu} = \frac{U \cdot D_h}{\nu}$$

- Hydraulic diameter

$$D_h = \frac{4 \cdot \text{Area}}{\text{Perimeter}}$$

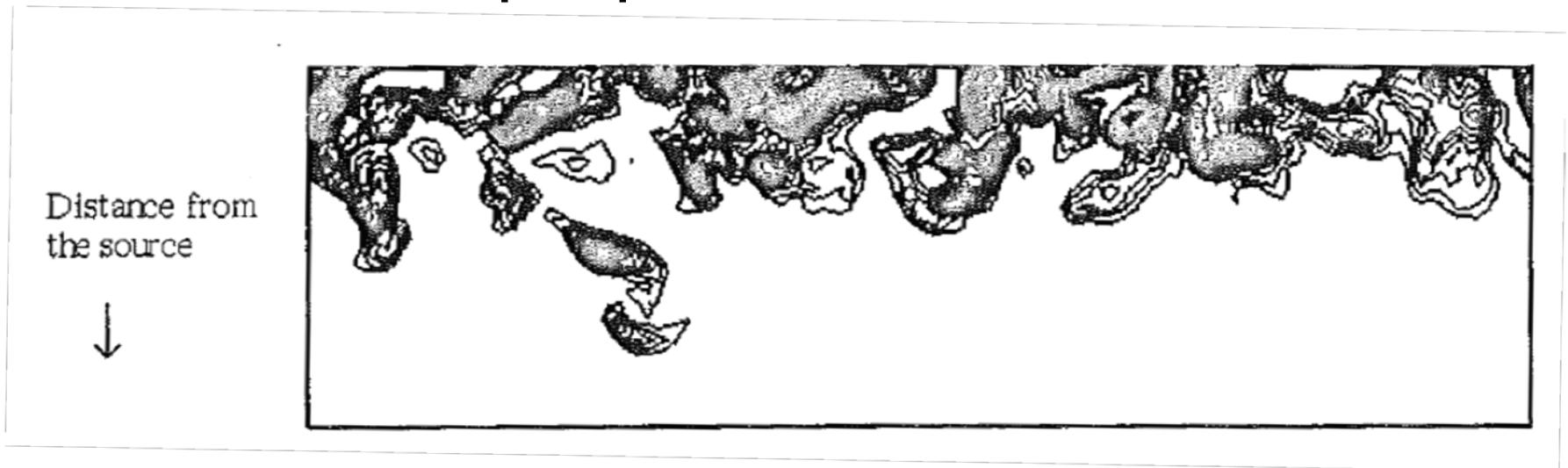
- Calculate the Reynolds number for a door:

- 0.8 m wide, 1.9 m in height
- U is 1.5 m/s, fluid is air at 20 °C
- The kinematic viscosity is

$$\nu = 1.51 \cdot 10^{-5}$$

Turbulence

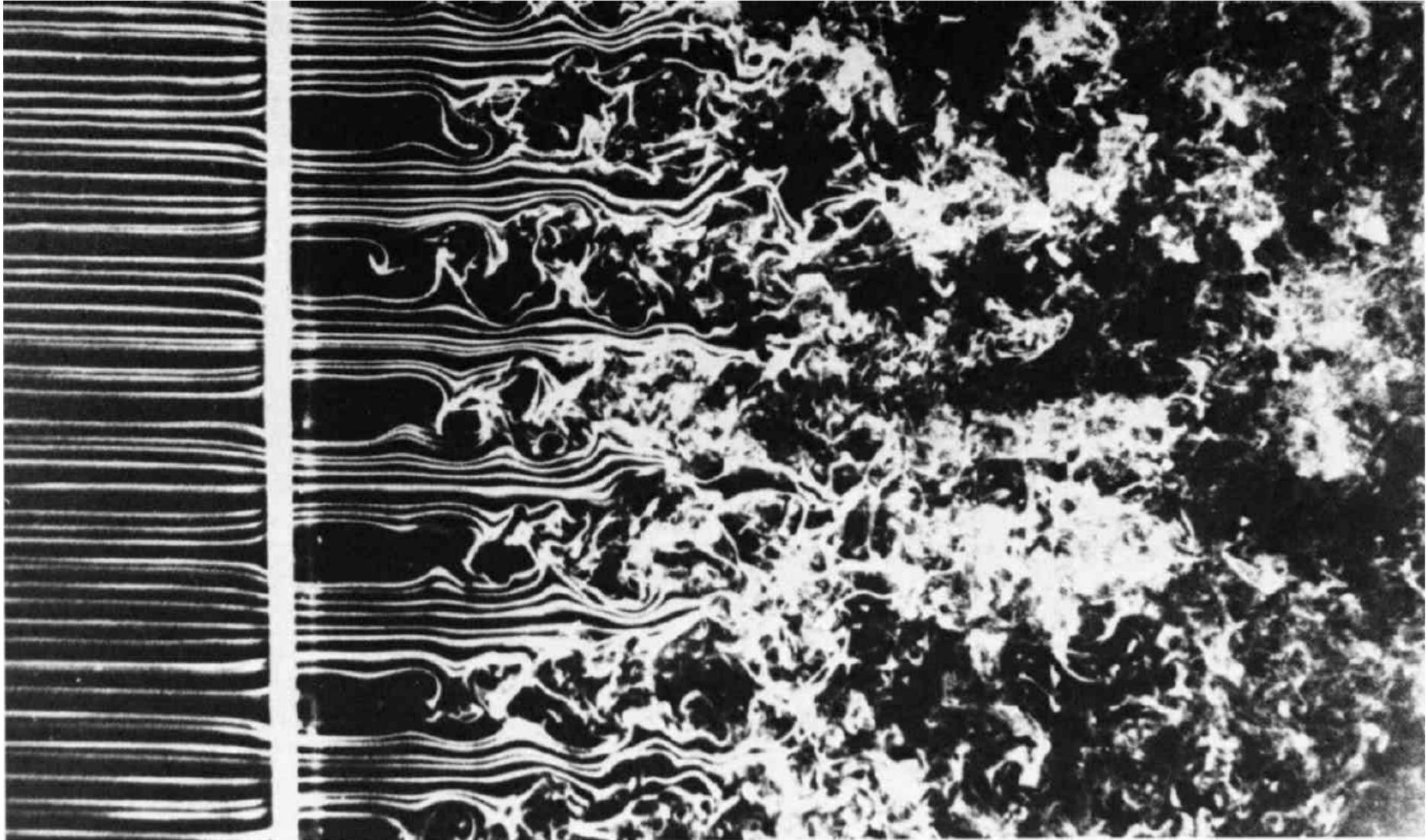
- Chaotic
- Anisotropic phenomena



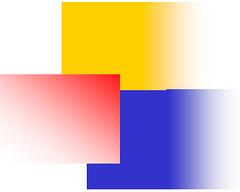
DNS Simulation. Contours of the kinetic energy on a plane in the flow created by an oscillating grid in a quiescent fluid; the grid is located at the top of the figure.

Generation of turbulence by a grid

6 grid holes of $\frac{3}{4}$ inch (19.05 mm) can be seen at the left side



Source: Van Dyke, *An Album of Fluid Motion*, Stanford, 1982 (p. 89)



Turbulent water jet
directed downward into
water seen in the plane of
symmetry. The jet is
illuminated by using Laser-
induced fluorescence (LIF).

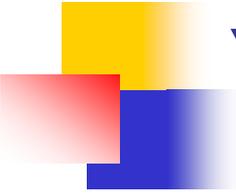


Source: Van Dyke, *An Album of Fluid Motion*, Stanford, 1982 (page 97)

Comparison of laminar and turbulent boundary layer separation

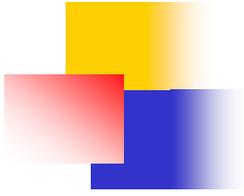
Laminar at top separates and turbulent at bottom stays attached





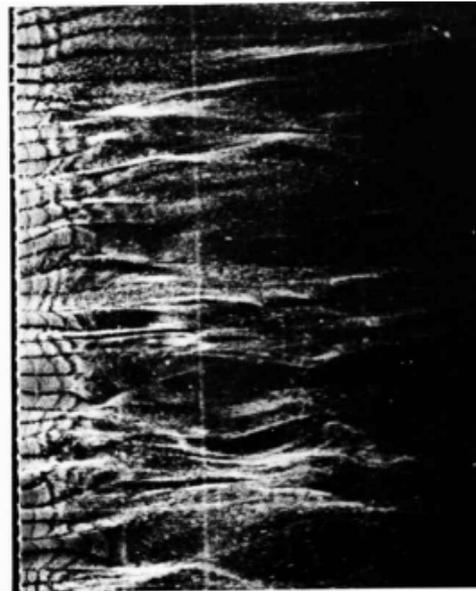
Y_+

- Y_+ is a ratio between turbulent and laminar influences in a cell, if Y_+ is big then the cell is turbulent, if it is small it is laminar.
- This is from CFD online – a good forum.
- <https://www.cfd-online.com/Forums/main/861-can-someone-explain-y-plus-value.html>



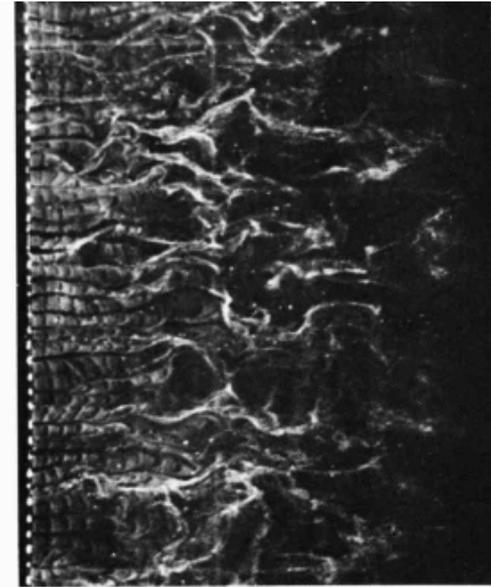
Structure of a turbulent boundary layer near a flat plate

$y^+ = 2.7$



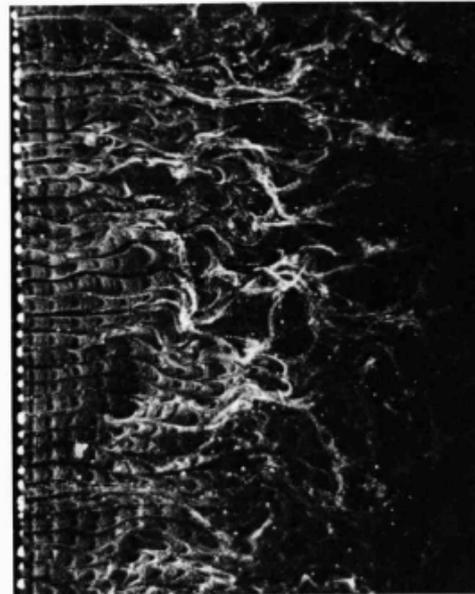
$y^+ = 2.7$

$y^+ = 38$



$y^+ = 38$

$y^+ = 101$



$y^+ = 101$

$y^+ = 407$

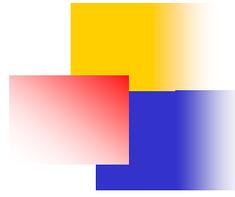


$y^+ = 407$

Creation of instabilities (Kelvin–Helmholtz instability)

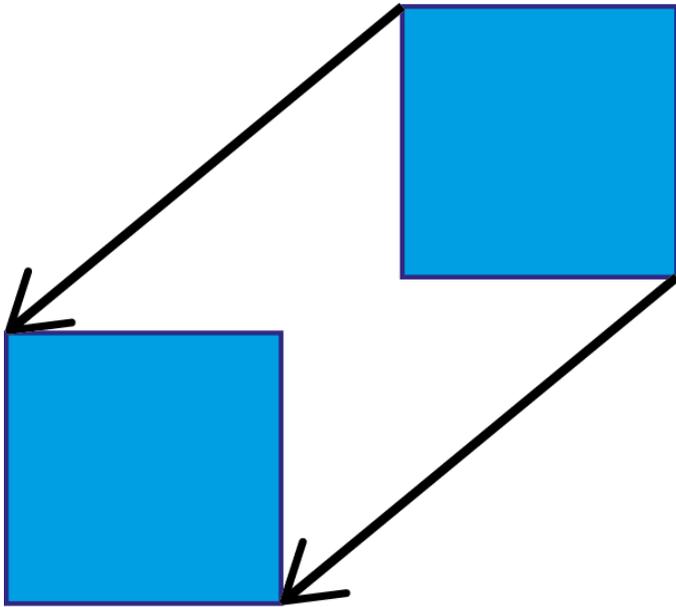


Source <https://de.wikipedia.org/wiki/Kelvin-Helmholtz-Instabilit%C3%A4t>

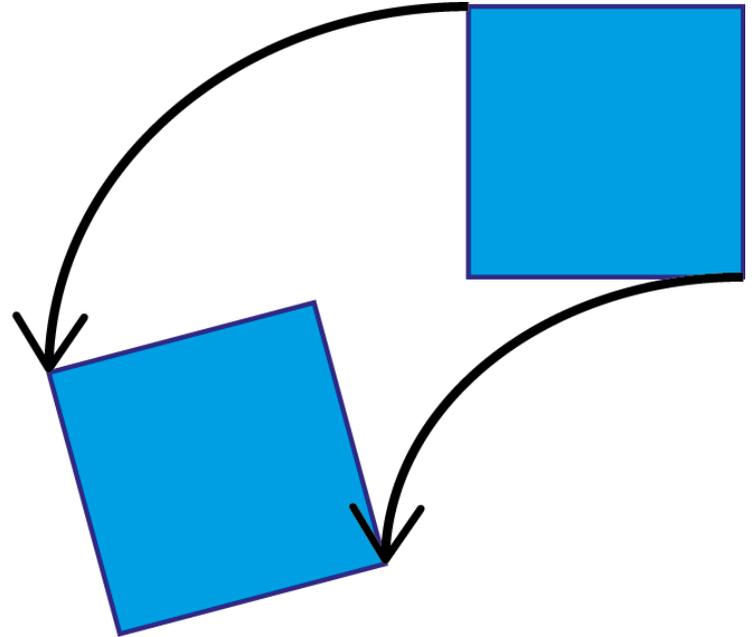


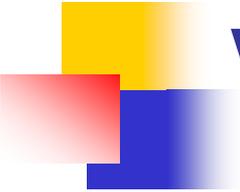
Vorticity

Translation



Rotation





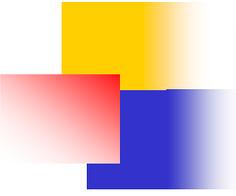
Vortex stretching

- Youtube

- <http://youtu.be/JaABLY6E8HE>

- http://youtu.be/59LL_IRs1MQ

- <https://youtu.be/Tfi8BLca07M> (5 min)



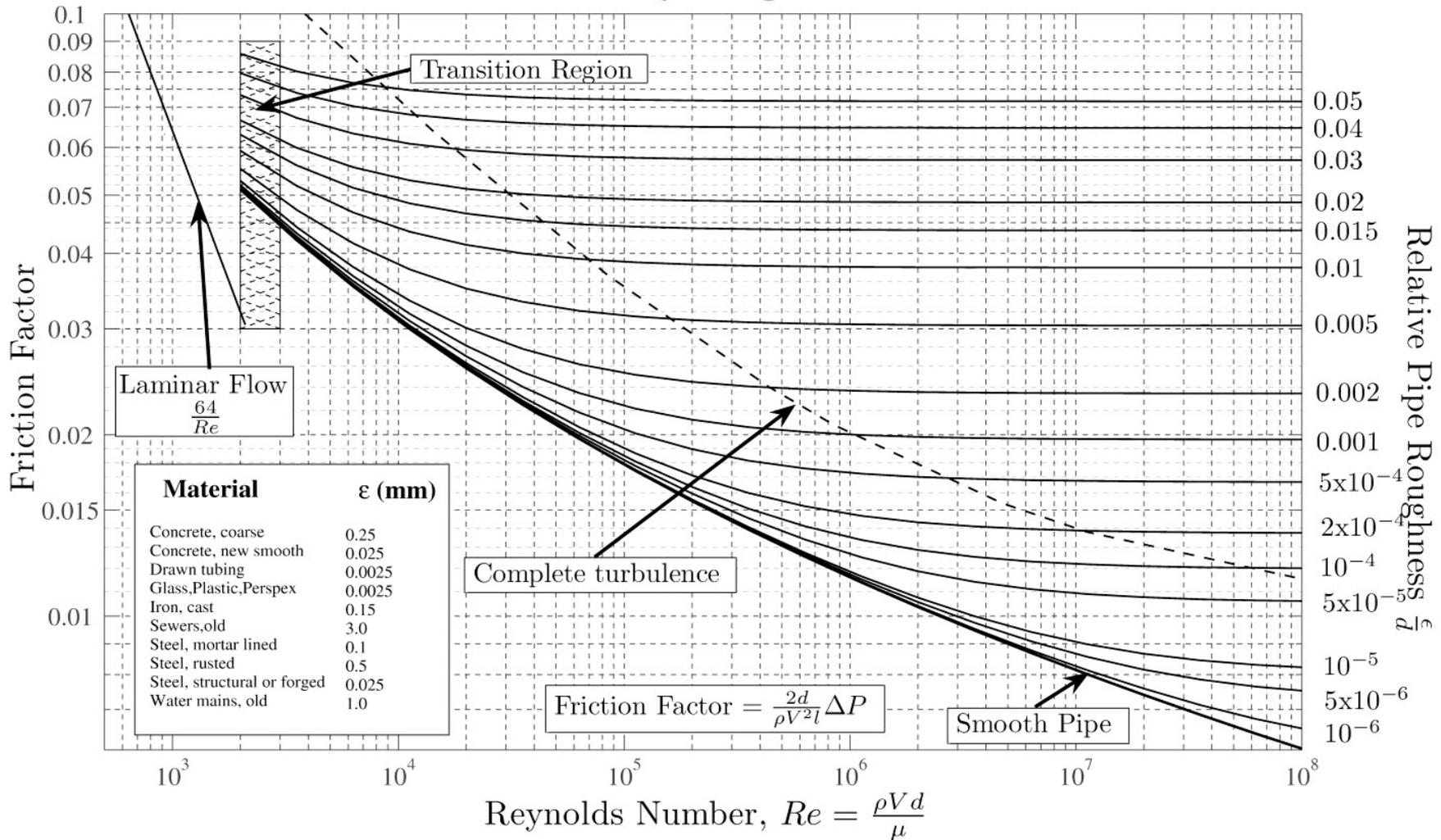
Hierarchy of turbulence models

- Simple models (eg. Moody chart, heat transfer)
 - 0. equation models (eg. Baldwin-Lomax for aerodynamic)
 - RANS models
 - LES models
 - DNS
-
- Further down on list – longer time to calculate

Turbulence in pipe flow

$$\Delta P = f \frac{\rho \cdot V^2 \cdot l}{2 \cdot d}$$

Moody Diagram

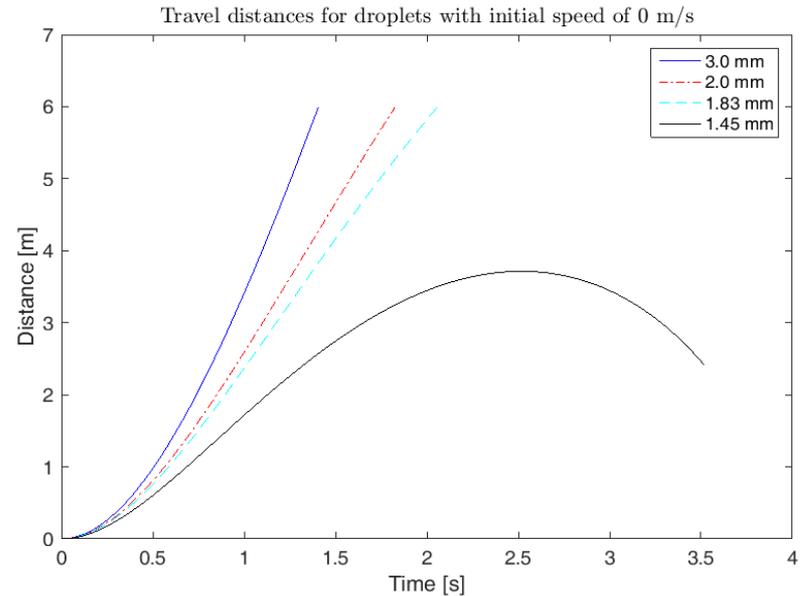


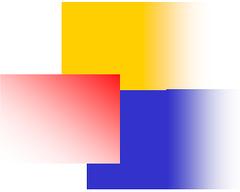
Example with Nusselt number for a failing droplet in hot air

$$\frac{dd}{dt} = \frac{2 \cdot h \cdot \Delta T}{H_v \cdot \rho}$$

$$h = \frac{Nu \cdot k}{d}$$

$$Nu = 2 + 0.6 \cdot Re^{0.5} \cdot Pr^{0.33}$$





Modelling of turbulence in CFD

- RANS (Reynolds Average Navier Stokes)
- LES (Large Eddy Simulation)
- DNS (Direct Numerical Simulation)

RANS - Mean Values

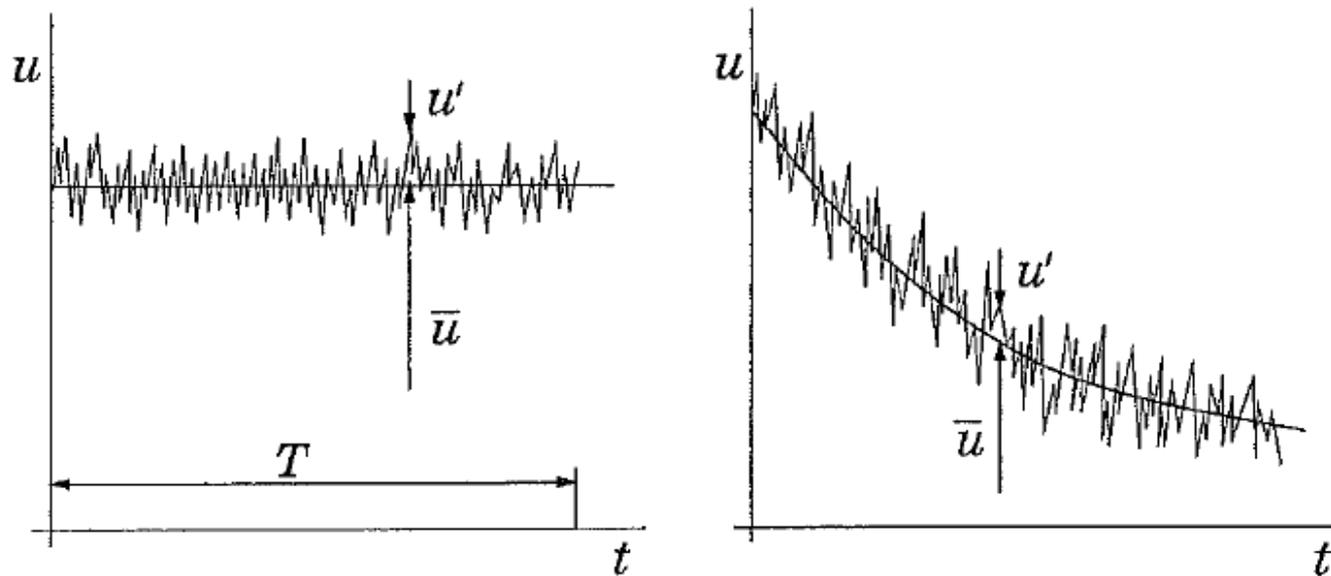
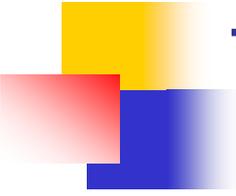


Fig. 9.10. Time averaging for a statistically steady flow (left) and ensemble averaging for an unsteady flow (right)



Turbulent kinetic energy

- For a quasi steady state flow the instantaneous velocity is the mean velocity + a fluctuating component

$$\mathbf{u} = \bar{\mathbf{u}} + \mathbf{u}'$$

- The turbulent kinetic energy k is defined as

$$k = \frac{1}{2} \left(\overline{u'^2} + \overline{v'^2} + \overline{w'^2} \right)$$

- The turbulent intensity is defined as

$$I = \frac{\sqrt{\frac{1}{3} \cdot \left(\overline{u'^2} + \overline{v'^2} + \overline{w'^2} \right)}}{\bar{u}}$$

LES and DNS, Ferziger and Peric (2002)

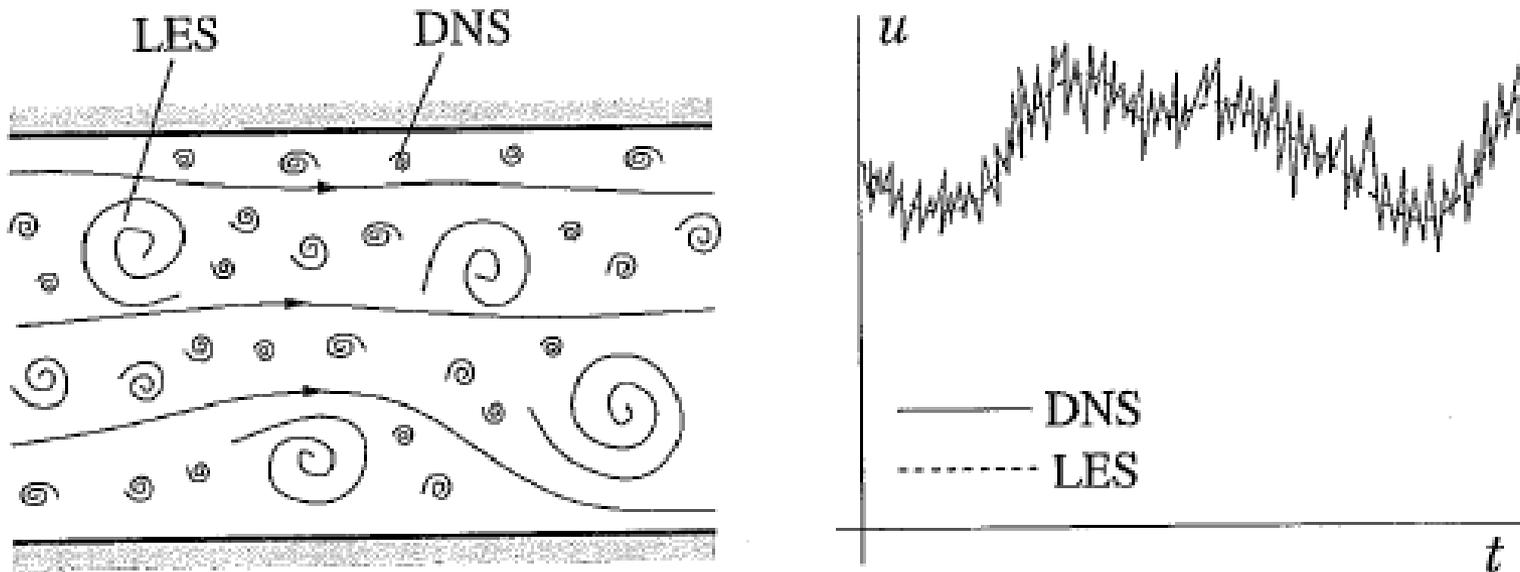
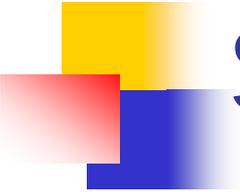


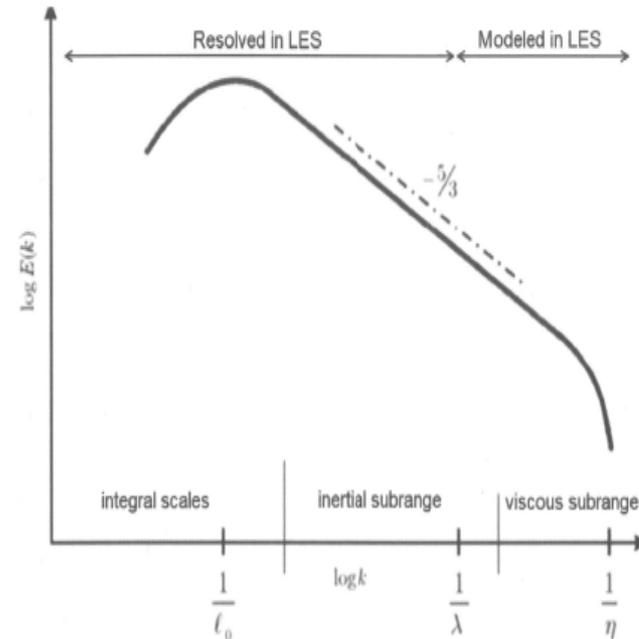
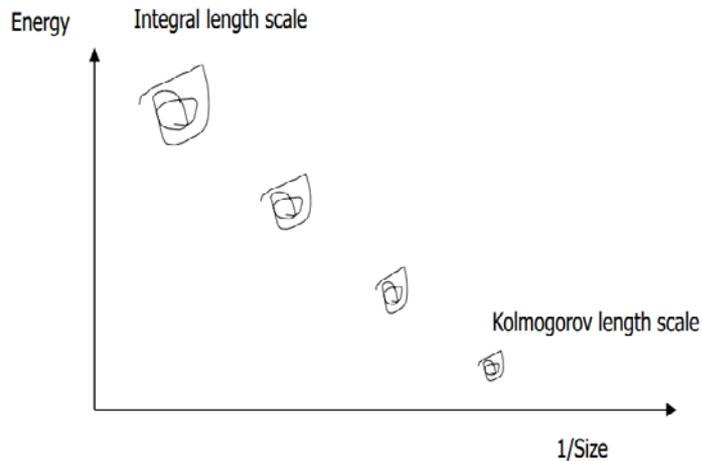
Fig. 9.3. Schematic representation of turbulent motion (left) and the time dependence of a velocity component at a point (right)



Scales of turbulent structures

- Integral scale – largest scale
- Taylor micro scale – Viscosity starts to become important
- Kolmogorov scale – smallest turbulent scale.

Using Turbulence resolution (amount of unresolved turbulent kinetic energy)



Picture: Per Petersson

$$mtr = \frac{k_{subgrid}}{k_{LES} + k_{subgrid}}$$

RANS

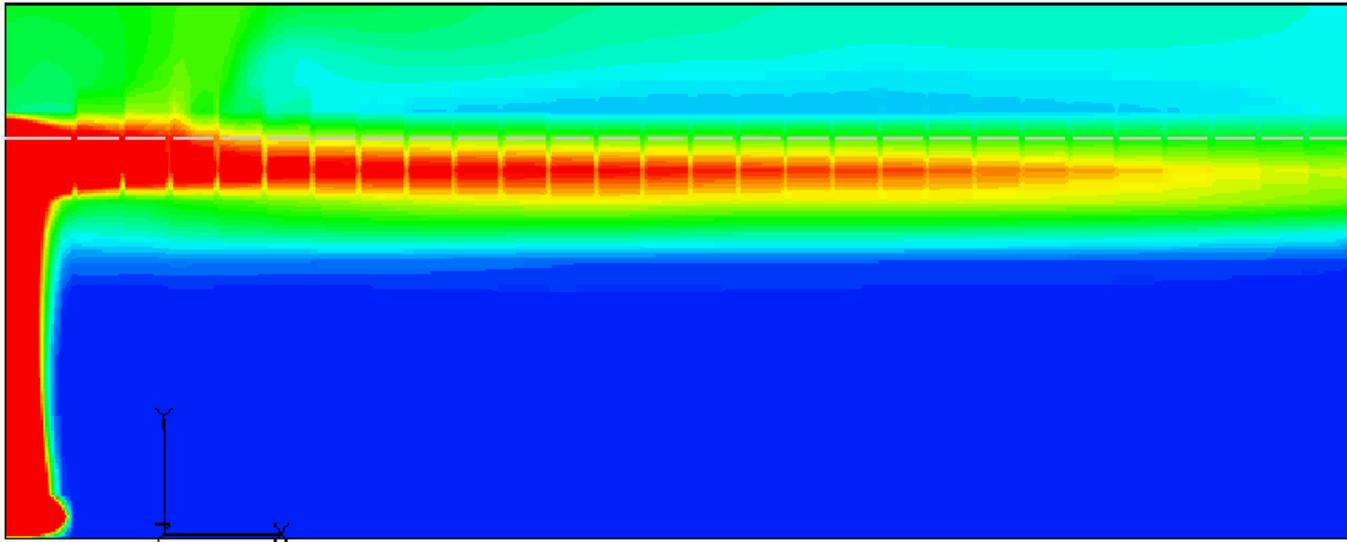
- Reynolds Average Navier Stokes

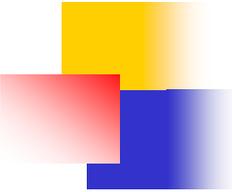
$$\mathbf{u} = \bar{\mathbf{u}} + \mathbf{u}' \quad \text{velocity}$$

$$u' = \sqrt{\frac{1}{3} (u'_x{}^2 + u'_y{}^2 + u'_z{}^2)} \quad \text{flutuatic velocity}$$

$$I \equiv \frac{u'}{\bar{u}} \cdot 100\% \quad \text{turbulent intensity}$$

Mean value picture

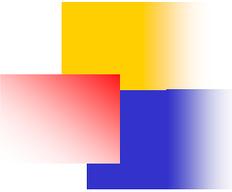




RANS 2

$$\tau_{i,j} = \rho \overline{u'_i u'_j} = \rho \begin{pmatrix} \overline{u'_1 u'_1} & \overline{u'_1 u'_2} & \overline{u'_1 u'_3} \\ \overline{u'_2 u'_1} & \overline{u'_2 u'_2} & \overline{u'_2 u'_3} \\ \overline{u'_3 u'_1} & \overline{u'_3 u'_2} & \overline{u'_3 u'_3} \end{pmatrix}$$

- Turbulence models with RANS
 - Equations are averages
 - But there are too few equations to the number of unknown variables (this is called Closure)
 - Therefore additional equations are needed to close the system of equations



RANS 3

- Most well-known model to close the RANS equation is

- k- ε model

- k is turbulent kinetic energy

$$k = \frac{1}{2} \left(\overline{(u'_1)^2} + \overline{(u'_2)^2} + \overline{(u'_3)^2} \right).$$

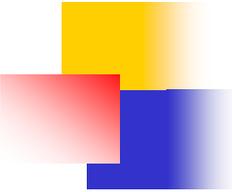
- ε is the turbulent dissipation

- Are used in industrial applications

- Other models

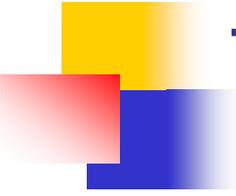
- k- ω model

- Menter model



RANS 4

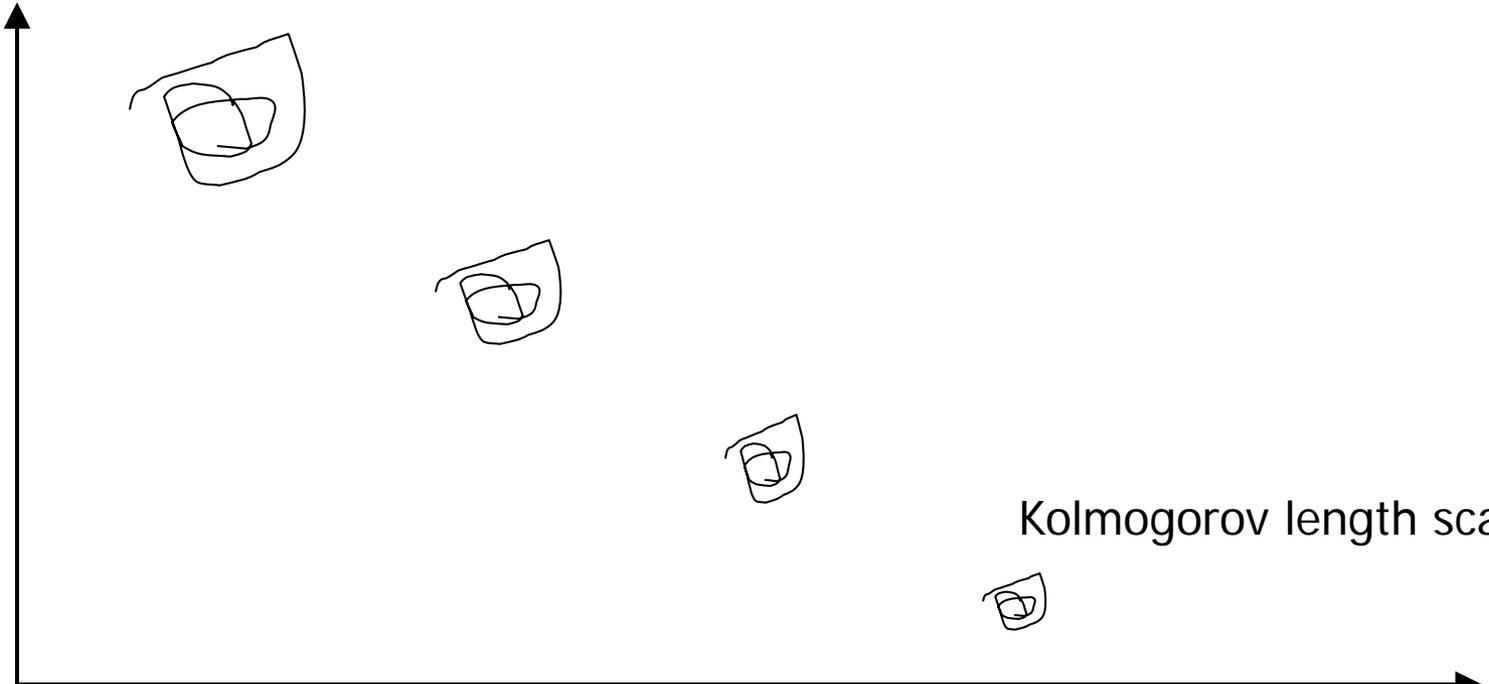
- The most time consuming closure for RANS is:
 - The Reynolds stress model
 - Gives 7 extra partial differential equations
 - Difficult to get to converge (solve)
 - It is maybe then better to use LES instead (see Versteeg, page 109)



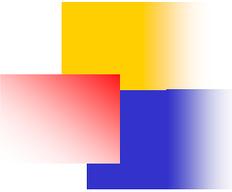
Turbulence cascade

Energy

Integral length scale

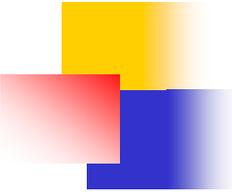


1/Size



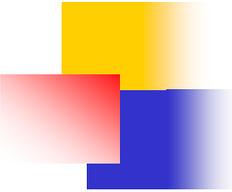
LES 1

- Filtering of the equations
 - Eddies below a given size Δ are handled by the "sub grid" model
 - $\Delta > h$, h is the grid size
 - Model to handle the "small" eddies, turbulent viscosity
 - Constant Smagorinsky
 - Dynamic Smagorinsky
 - Deardorff (Default in FDS 6)
 - Vreman



LES 2

- Energy on sub-grid
 - 90 % of the eddies should be resolved in the large grid, (se Combustion af Warnatz, Maas og Dibble)
 - This is rarely the case when using FDS
 - Use Measurement of turbulent resolution



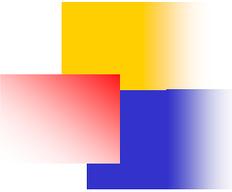
LES 3 Turbulent viscosity

- Smagorinsky

$$\mu_t = \rho (C_s \Delta)^2 |S| \quad ; \quad |S| = \left(2S_{ij}S_{ij} - \frac{2}{3}(\nabla \cdot \mathbf{u})^2 \right)^{\frac{1}{2}}$$

- Deardorff

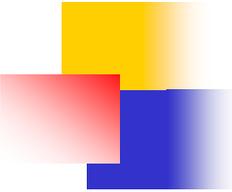
$$\mu_t = \rho C_v \Delta \sqrt{k_{sgs}} \quad ; \quad k_{sgs} = \frac{1}{2} ((\bar{u} - \hat{u})^2 + (\bar{v} - \hat{v})^2 + (\bar{w} - \hat{w})^2)$$



LES 4

- Setting turbulence model in FDS

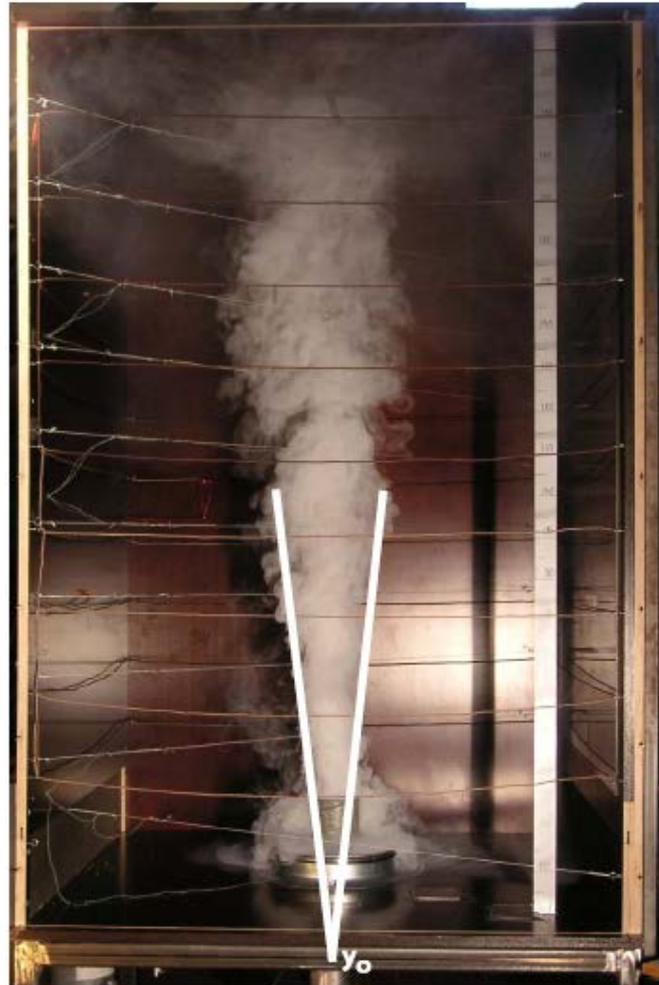
TURBULENCE_MODEL	Description	Coefficient(s)
'CONSTANT SMAGORINSKY'	Constant coefficient Smagorinsky model [11]	C_SMAGORINSKY
'DYNAMIC SMAGORINSKY'	Dynamic Smagorinsky model [12, 13]	None
'DEARDORFF'	Deardorff model [9, 10]	C_DEARDORFF
'VREMAN'	Vreman's eddy viscosity model [14]	C_VREMAN
'RNG'	Renormalization group eddy viscosity model [15]	C_RNG, C_RNG_CUTOFF



Smagorinsky constant (C_s)

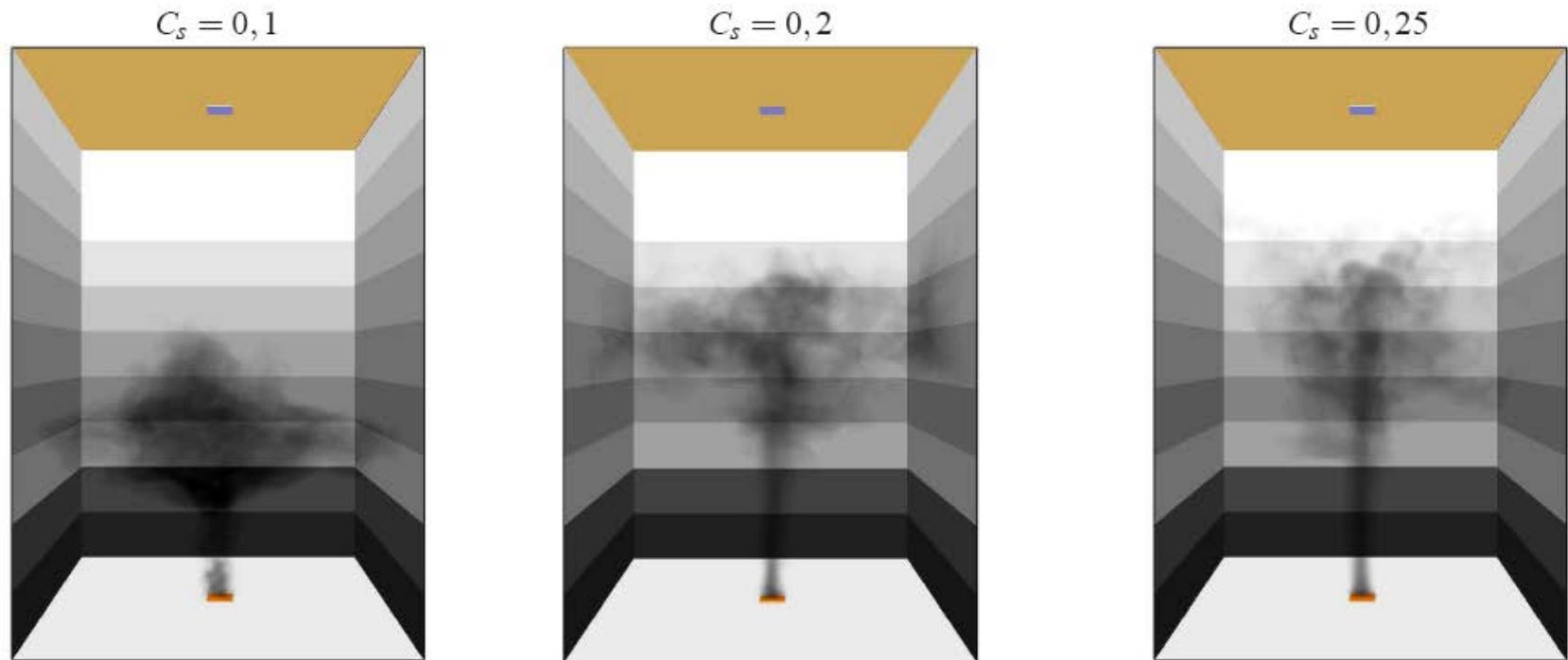
- What should it be (FDS 5)
 - It is set to 0.20, but it depends on the geometry
- Example from Sommerlund-Larsen and Petersen's, M.Sc. Thesis
- FDS 6 uses a dynamic Smagorinsky model

Experiment – Sommerlund-Larsen and Petersen



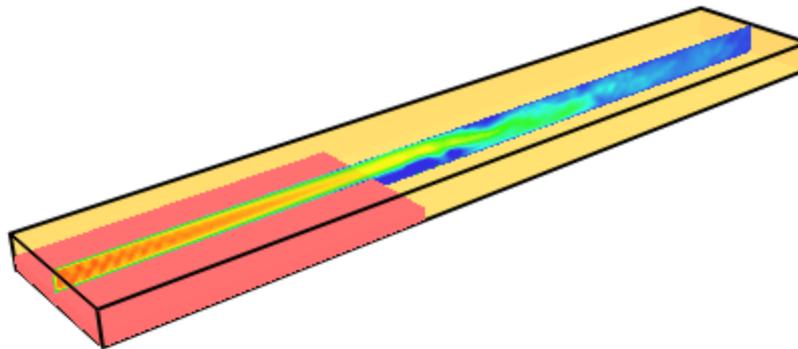
Plumen under forsøg med opdriftsneutralt røglag, hvor spredningsvinklen er fundet til 14° .

Different value of C_s (Fixed Smagorinsky constant)

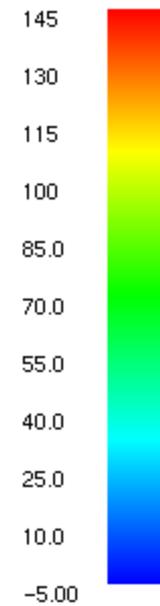


Figur M.11: Røglagets udvikling efter 40 sekunders 14x14 cm 50 W brand. De tre brande har forskellige Smagorinsky konstanter; og fra venstre af, antager de værdierne 0,1, 0,2 og 0,25.

Backward facing step



Slice
U-VEL
m/s
 $\times 10^{-2}$

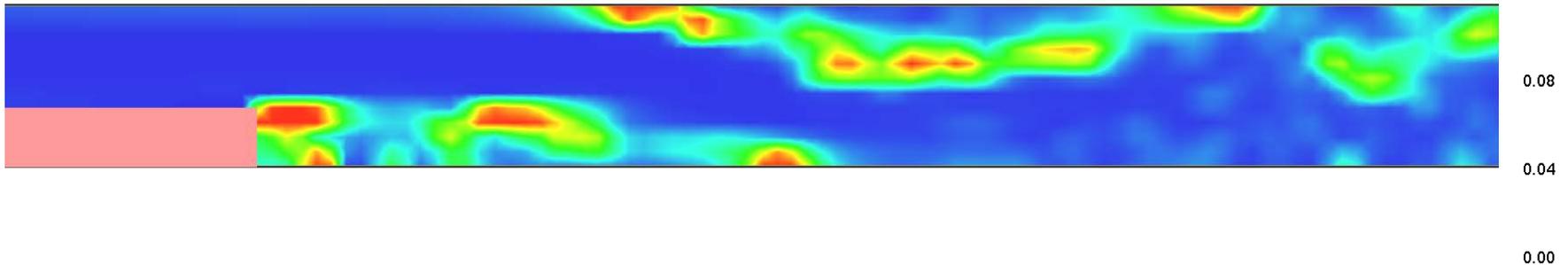


Time: 16.18



Dynamic Smagorinsky constant

- Backward facing step
 - Shows the amount of turbulent energy that are resolved
 - Larger blue area is better (means less energy is handled by the Smagorinsky model)



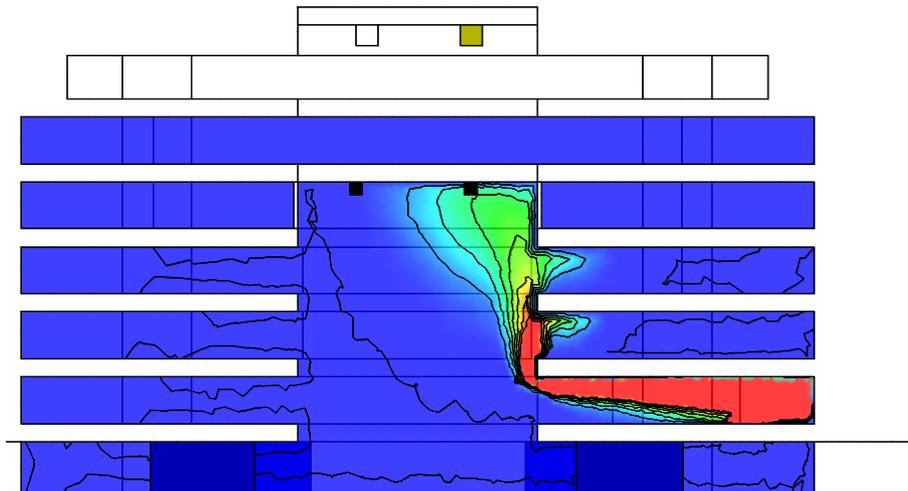
RANS versus LES

Kontorhus med atrium

1 MW fast brand – mekanisk udsugning

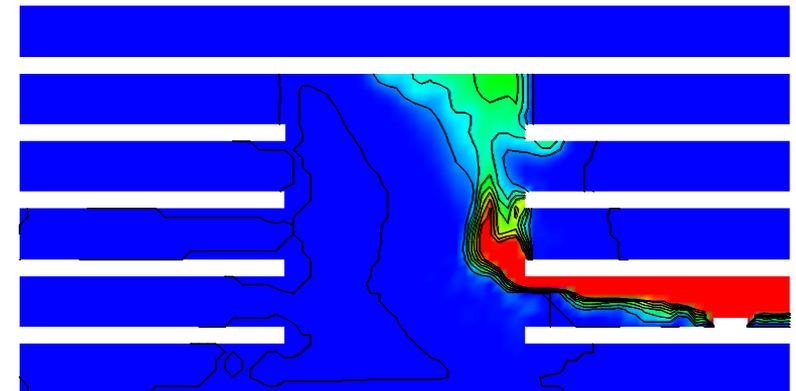
90 sekunder

RANS model



CFX 5.7

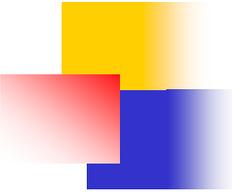
LES model



FDS 4.03

Temperatur





Pope's questions

- 1. Is LES the right approach?
- 2. Can the resolution of all scales be made tractable?
- 3. Do we have sufficient computer power for LES?
- 4. Is LES a physical model, a numerical procedure or a combination of both?
- 5. How can LES be made complete? (MTR)
- 6. What is the relationship between U and W ?
- 7. How do predicted flow statistics depend on ?
- 8. What is the goal of an LES calculation?
- 9. How are different LES models to be appraised?
- 10. Why is the dynamic procedure successful?

Statistic, question 7

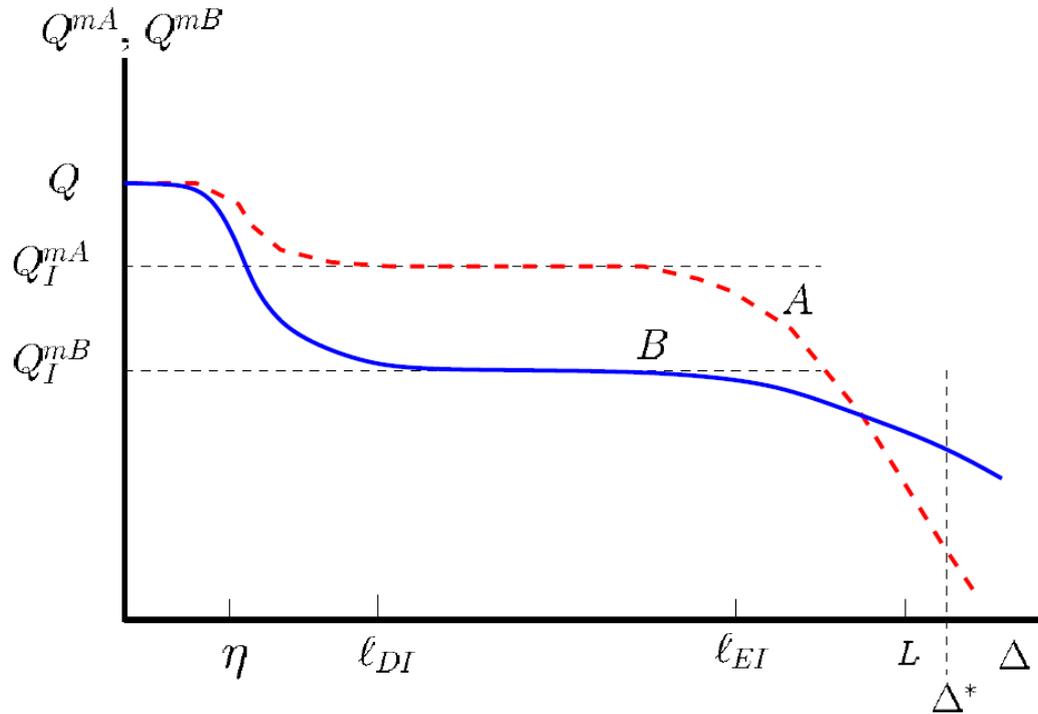


Figure 5. The predictions $Q^{mA}(\Delta)$ and $Q^{mB}(\Delta)$ of the statistic Q obtained from LES models A and B as functions of the turbulence resolution length scale Δ for the case in which Q has contributions from both energy-containing and dissipative scales.