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# Turbulence

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**LUND**  
UNIVERSITY

# Fire in wind mill, Denmark, 4. august 2017





# Purpose of lecture

Why is the understanding of turbulence important

- Turbulence is responsible in fires
  - Rate for combustion (mixing)  $Da = \frac{\text{flow time scale}}{\text{chemical time scale}}$
  - Entrainment in fire plumes
  - Flow around obstacles
- Explosion
  - Faster mixing, video <https://youtu.be/PdfY3EDrGrQ>
    - Deflagration > Detonation



# Overview

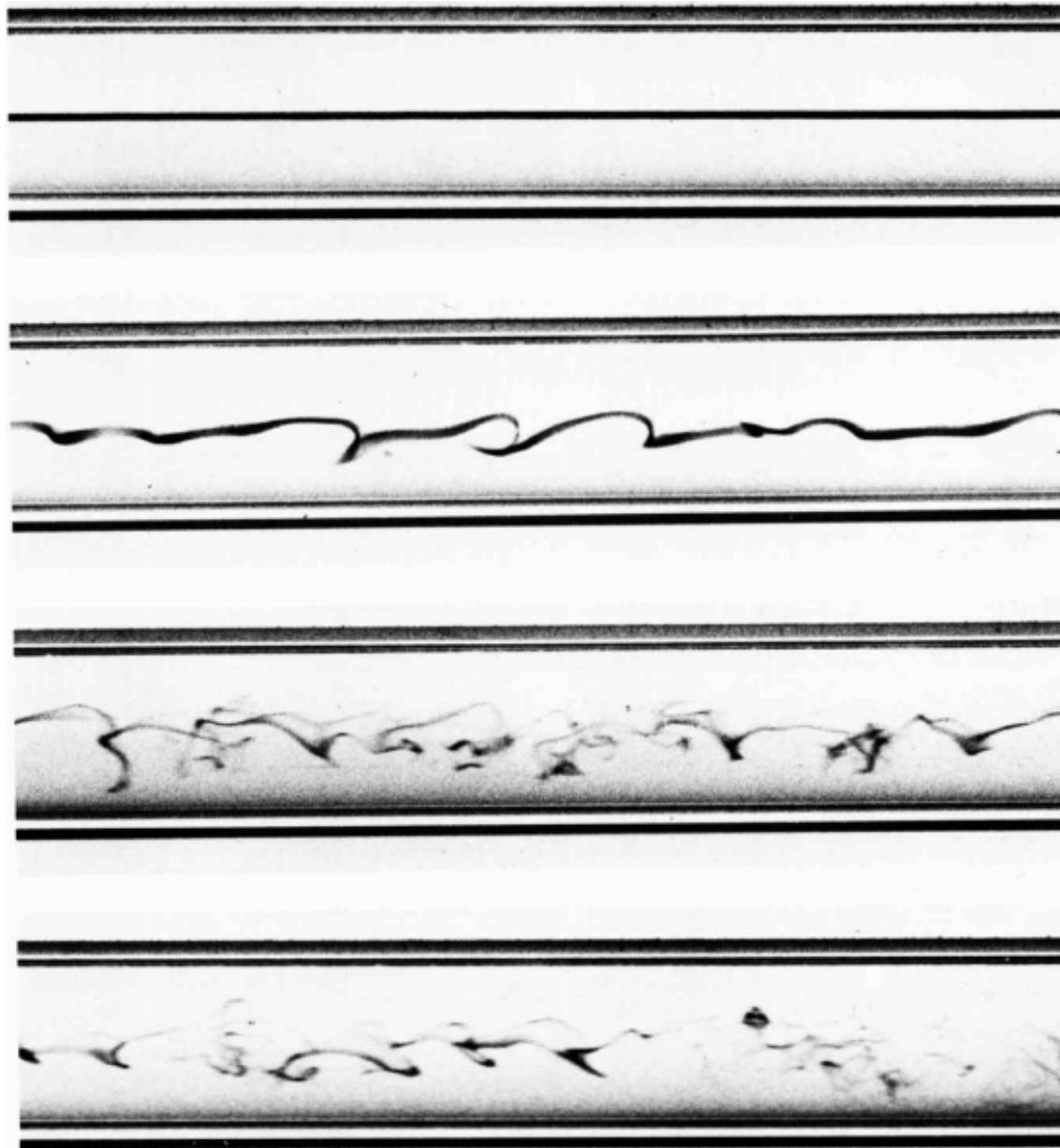
- Laminar and turbulent flow
- What is turbulence
- Reynolds number
- Transition from laminar to turbulent flow
- Treatment of turbulence in CFD codes
  - RANS
  - LES
  - DNS



# Laminar and turbulent flow

- Most flow of interest are turbulent
  - Flow in pipes
  - Mixing process (eg. pharmaceutical industry)
  - Fires
- Transition between laminar and turbulent flow can be determined by the Reynolds number. For a pipe flow the transition happens between 2000 – 3000. Flow over a plate:  $Re_x \approx 5 \cdot 10^5$

# Repetition of Osborne Reynolds dye experiment from 1883



Source: Van Dyke, An Album of Fluid Motion, Stanford, 1982 (p. 61)



# Find the Reynolds number

- Definition

$$Re = \frac{\rho \cdot U \cdot D_h}{\mu} = \frac{U \cdot D_h}{\nu}$$

- Hydraulic diameter

$$D_h = \frac{4 \cdot \text{Area}}{\text{Perimeter}}$$

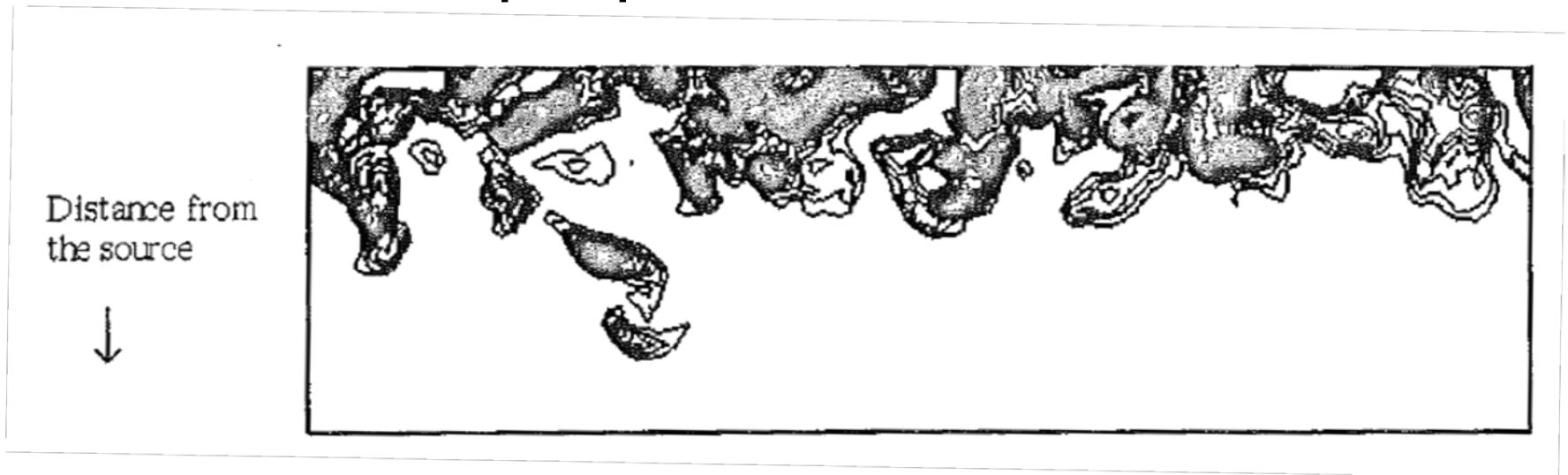
- Calculate the Reynolds number for a door:

- 0.8 m wide, 1.9 m in height
- U is 1.5 m/s, fluid is air at 20 °C
- The kinematic viscosity is

$$\nu = 1.51 \cdot 10^{-5}$$

# Turbulence

- Chaotic
- Anisotropic phenomena

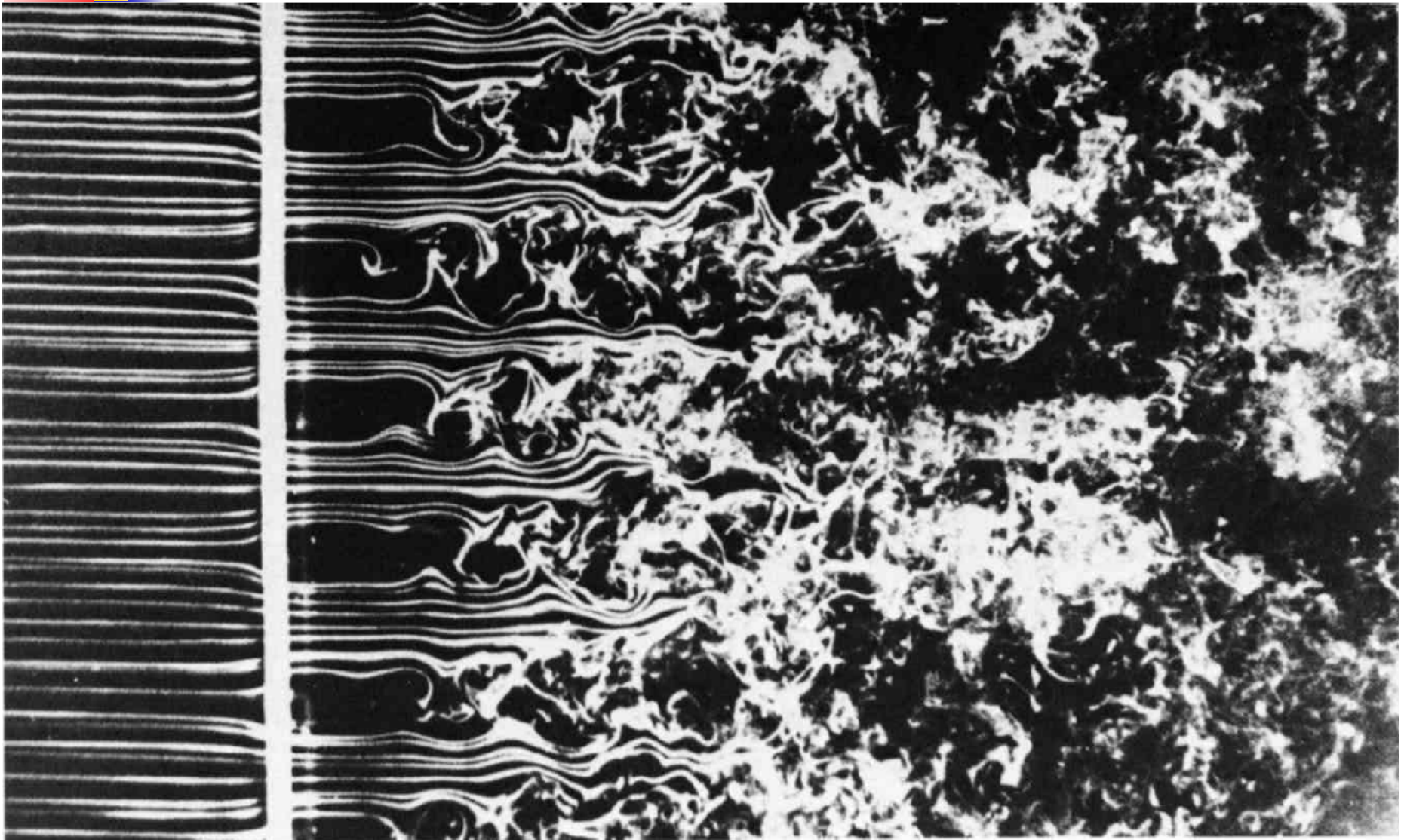


DNS Simulation. Contours of the kinetic energy on a plane in the flow created by an oscillating grid in a quiescent fluid; the grid is located at the top of the figure.




# Generation of turbulence by a grid

6 grid holes of  $\frac{3}{4}$  inch (19.05 mm) can be seen at the left side



Source: Van Dyke, An Album of Fluid Motion, Stanford, 1982 (p. 89)



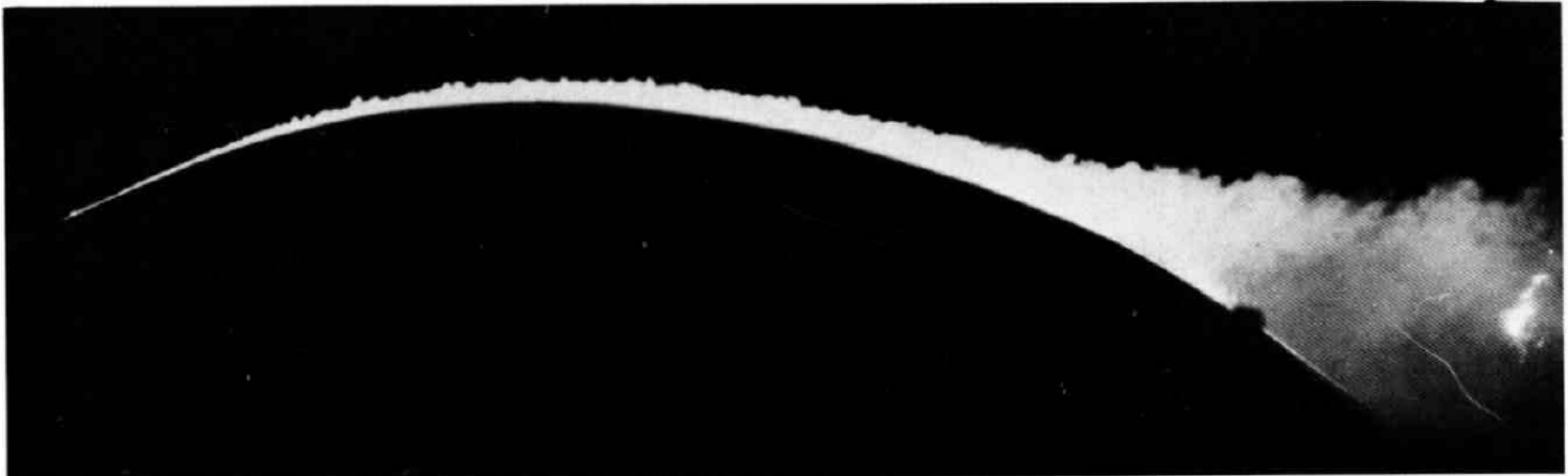
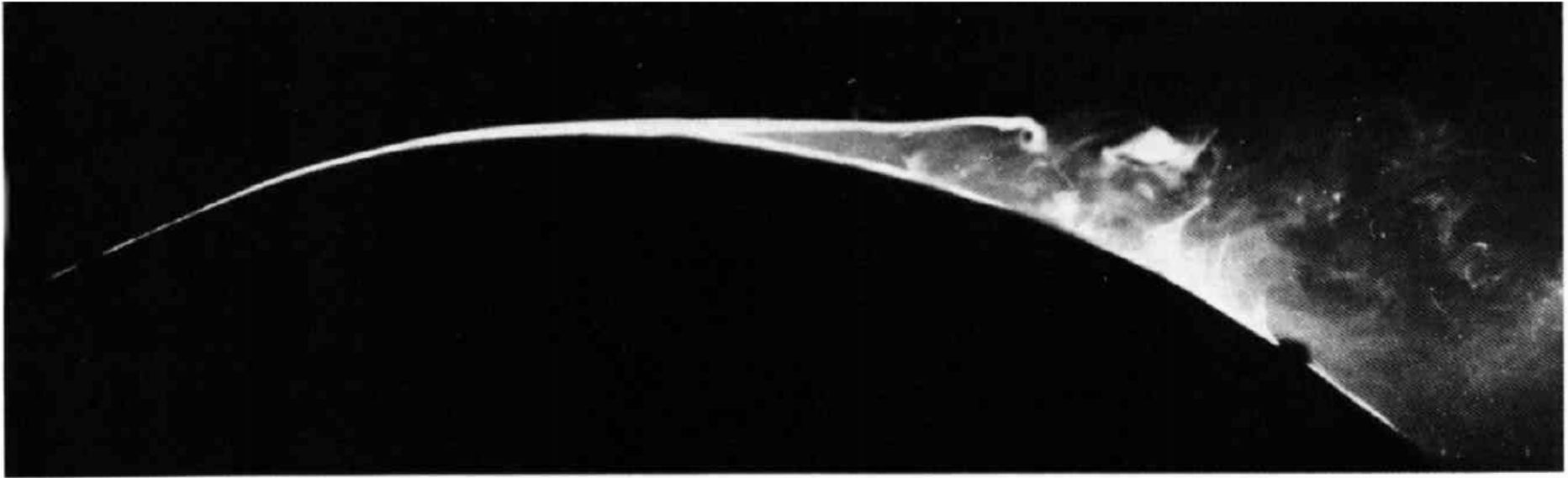
Turbulent water jet  
directed downward into  
water seen in the plane of  
symmetry. The jet is  
illuminated by using Laser-  
induced fluorescence (LIF).



Source: Van Dyke, *An Album of Fluid Motion*, Stanford, 1982 (page 97)

# Comparison of laminar and turbulent boundary layer separation

Laminar at top separates and turbulent at bottom stays attached





$Y^+$

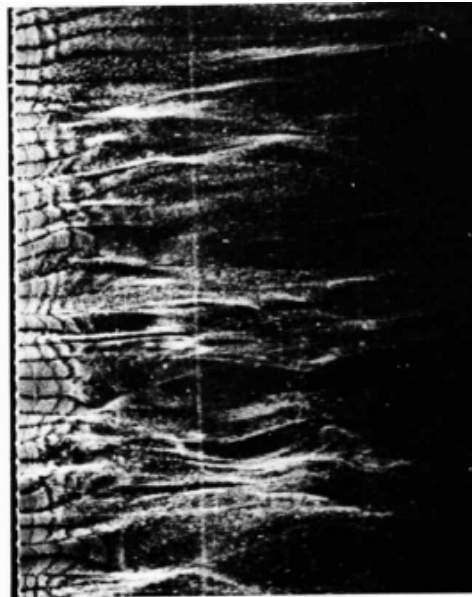
- $Y^+$  is a ratio between turbulent and laminar influences in a cell, if  $Y^+$  is big then the cell is turbulent, if it is small it is laminar.
- This is from CFD online – a good forum.
- <https://www.cfd-online.com/Forums/main/861-can-someone-explain-y-plus-value.html>





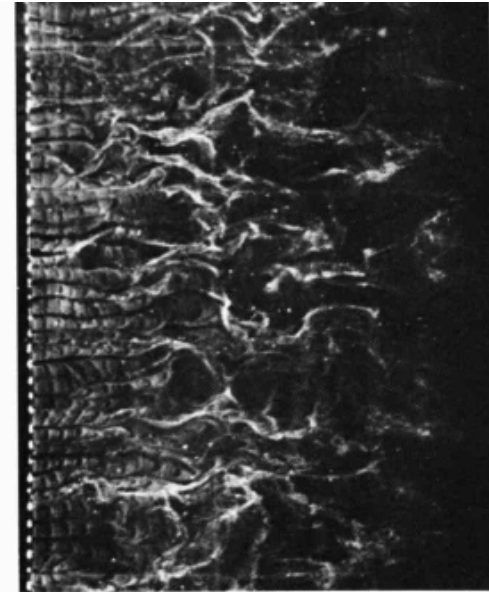
# Structure of a turbulent boundary layer near a flat plate

$y^+ = 2.7$



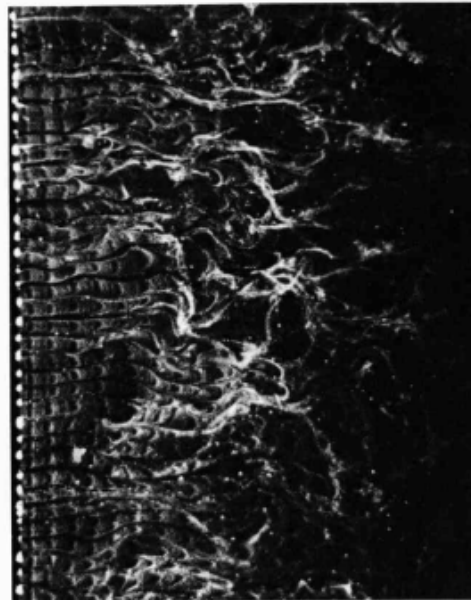
$y^+ = 2.7$

$y^+ = 38$



$y^+ = 38$

$y^+ = 101$



$y^+ = 101$

$y^+ = 407$



$y^+ = 407$

# Creation of instabilities

## (Kelvin–Helmholtz instability)

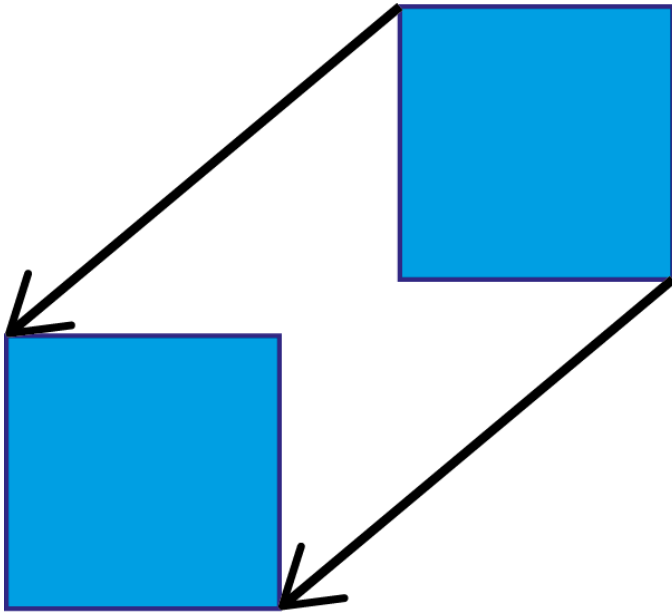


Source <https://de.wikipedia.org/wiki/Kelvin-Helmholtz-Instabilit%C3%A4t>

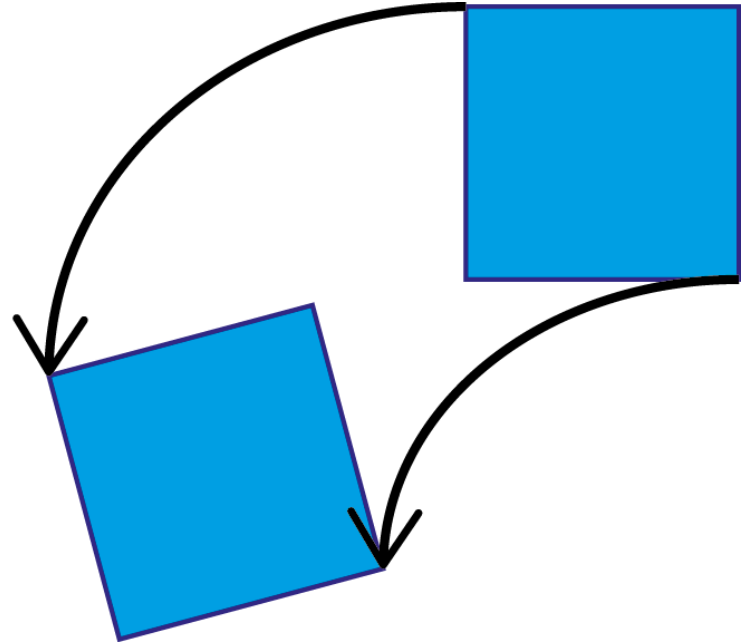


# Vorticity

Translation



Rotation





# Vortex stretching

- Youtube

- <http://youtu.be/JaABLY6E8HE>
- [http://youtu.be/59LL\\_IRs1MQ](http://youtu.be/59LL_IRs1MQ)
- <https://youtu.be/Tfi8BLca07M> (5 min)





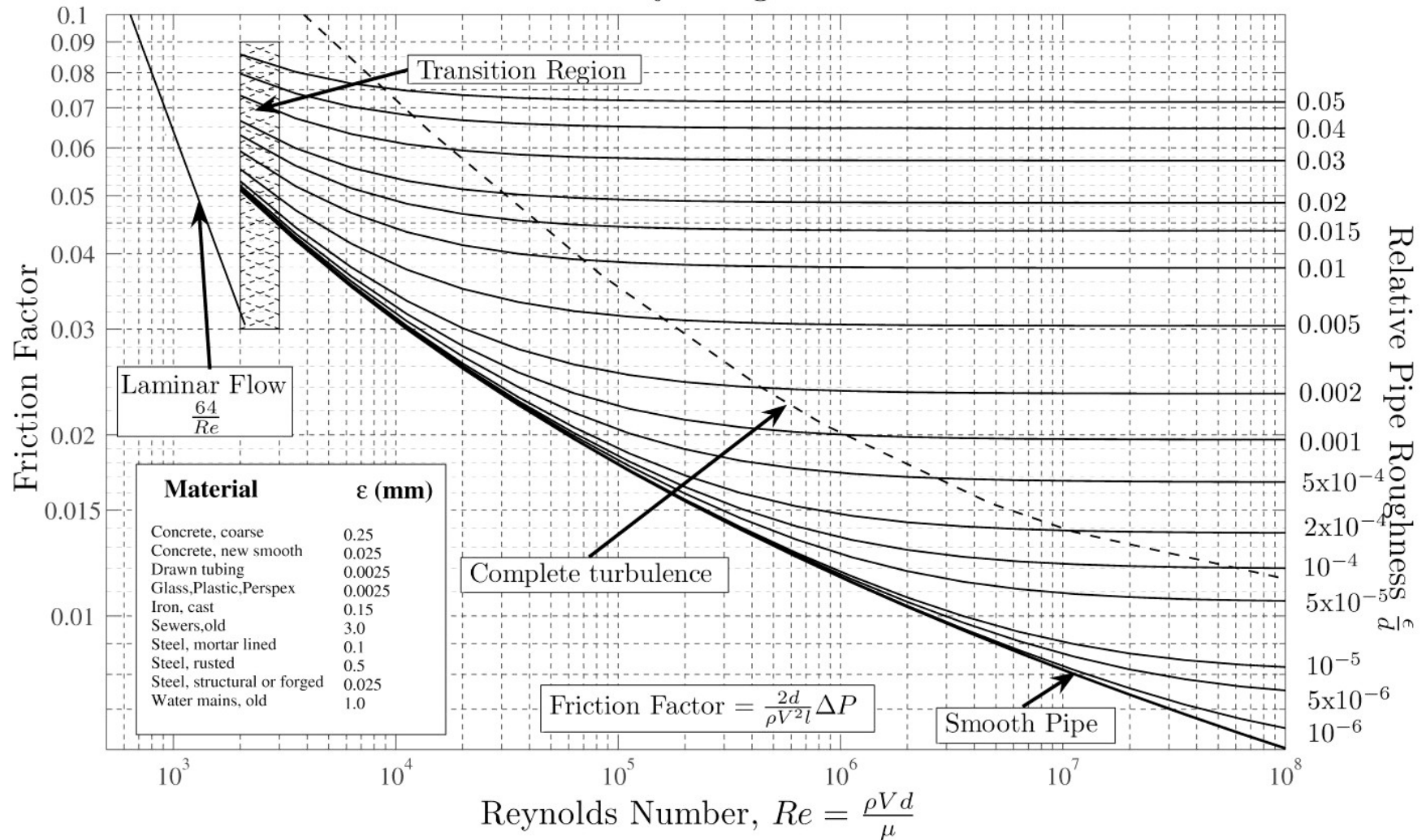
# Hierarchy of turbulence models

- Simple models (eg. Moody chart, heat transfer)
  - 0. equation models (eg. Baldwin-Lomax for aerodynamic)
  - RANS models
  - LES models
  - DNS
- 
- Further down on list – longer time to calculate

# Turbulence in pipe flow

$$\Delta P = f \frac{\rho \cdot V^2 \cdot l}{2 \cdot d}$$

Moody Diagram

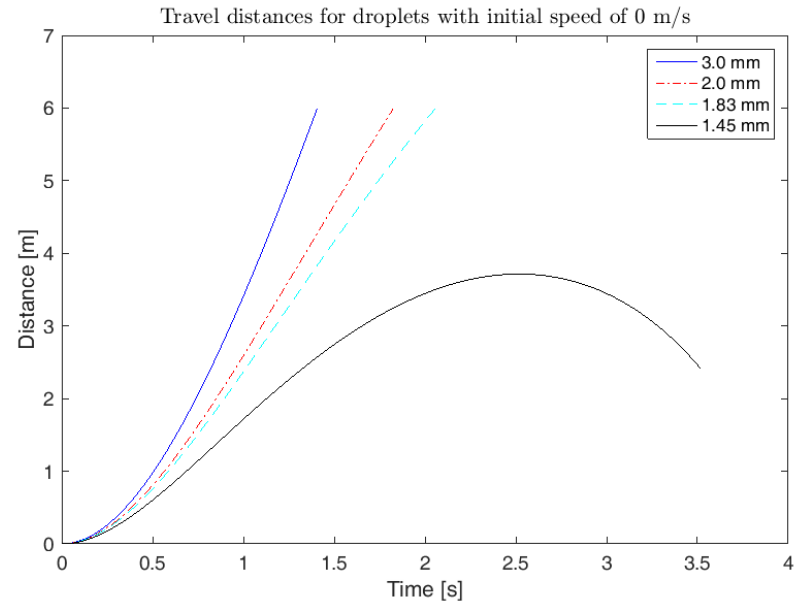


# Example with Nusselt number for a failing droplet in hot air

$$\frac{dd}{dt} = \frac{2 \cdot h \cdot \Delta T}{H_v \cdot \rho}$$

$$h = \frac{Nu \cdot k}{d}$$

$$Nu = 2 + 0.6 \cdot Re^{0.5} \cdot Pr^{0.33}$$

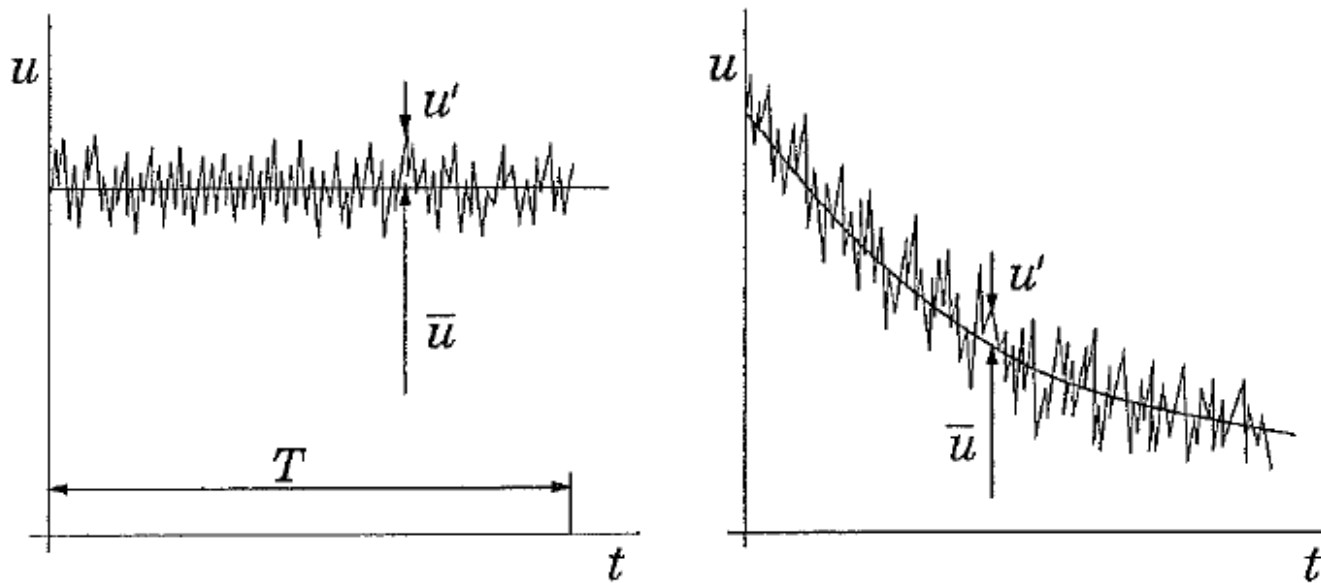




# Modelling of turbulence in CFD

- RANS (Reynolds Average Navier Stokes)
- LES (Large Eddy Simulation)
- DNS (Direct Numerical Simulation)

# RANS - Mean Values



**Fig. 9.10.** Time averaging for a statistically steady flow (left) and ensemble averaging for an unsteady flow (right)



# Turbulent kinetic energy

- For a quasi steady state flow the instantaneous velocity is the mean velocity + a fluctuating component

$$u = \bar{u} + u'$$

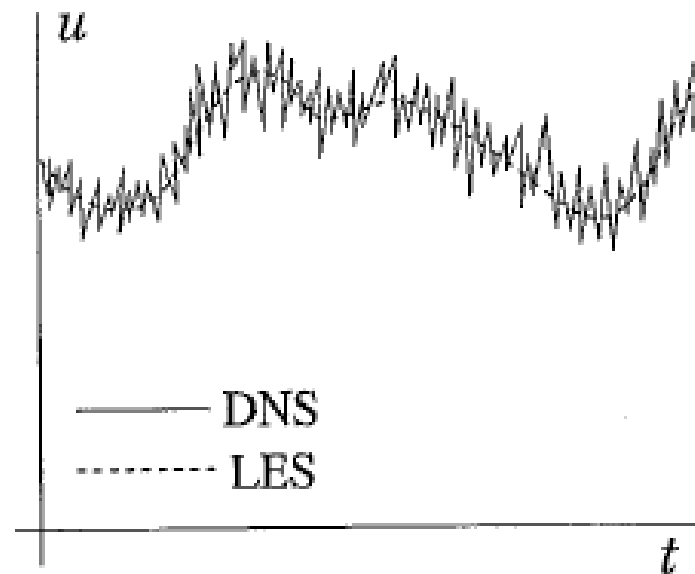
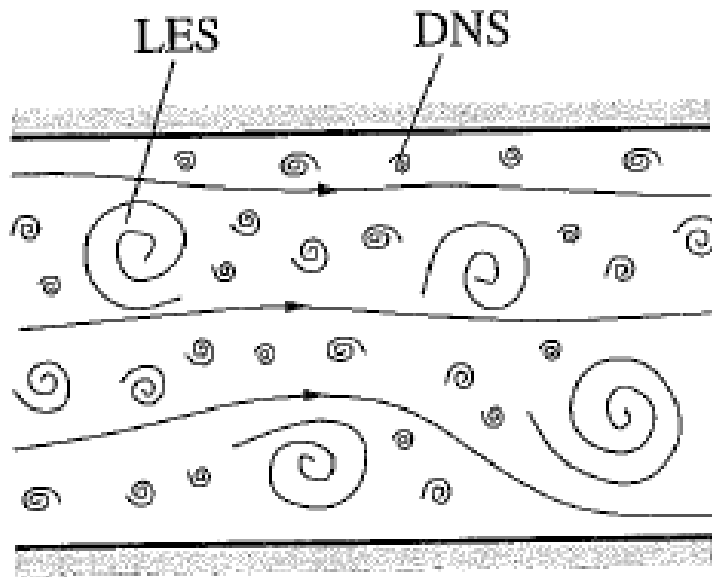
- The turbulent kinetic energy  $k$  is defined as

$$k = \frac{1}{2} \left( \overline{u'^2} + \overline{v'^2} + \overline{w'^2} \right)$$

- The turbulent intensity is defined as

$$I = \frac{\sqrt{\frac{1}{3} \cdot \left( \overline{u'^2} + \overline{v'^2} + \overline{w'^2} \right)}}{\bar{u}}$$

# LES and DNS, Ferziger and Peric (2002)



**Fig. 9.3.** Schematic representation of turbulent motion (left) and the time dependence of a velocity component at a point (right)

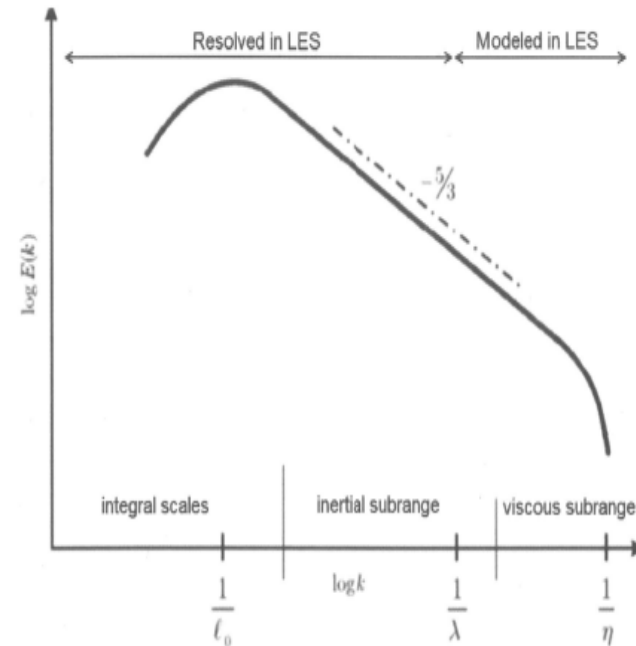
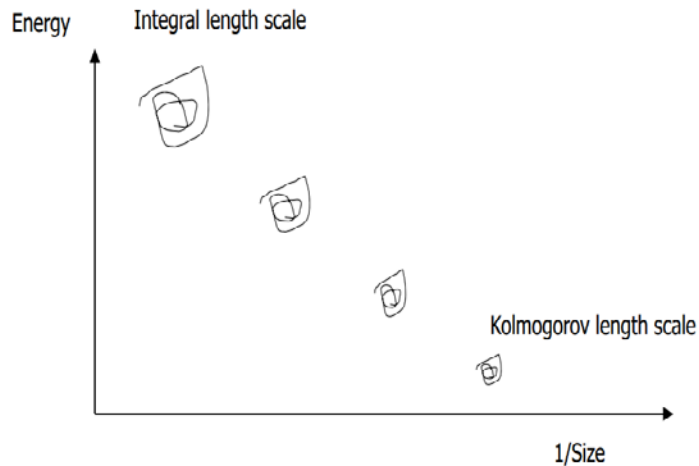


# Scales of turbulent structures

- Integral scale – largest scale
- Taylor micro scale – Viscosity starts to become important
- Kolmogorov scale – smallest turbulent scale.



# Using Turbulence resolution (amount of unresolved turbulent kinetic energy)



Picture: Per Petersson

$$mtr = \frac{k_{subgrid}}{k_{LES} + k_{subgrid}}$$

# RANS

## ■ Reynolds Average Navier Stokes

$$u = \bar{u} + u'$$

velocity

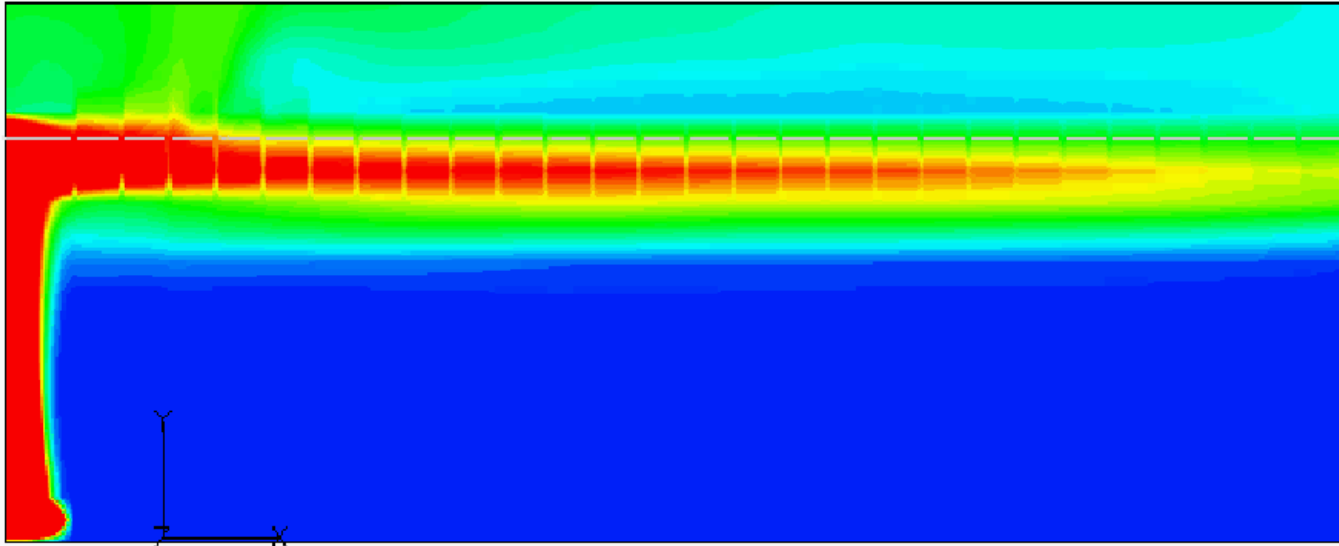
$$u' = \sqrt{\frac{1}{3} (u_x'^2 + u_y'^2 + u_z'^2)}$$

flutuatic velocity

$$I \equiv \frac{u'}{\bar{u}} \cdot 100\%$$

turbulent intensity

Mean value picture





# RANS 2

$$\tau_{i,j} = \rho \overline{u'_i u'_j} = \rho \begin{pmatrix} \overline{u'_1 u'_1} & \overline{u'_1 u'_2} & \overline{u'_1 u'_3} \\ \overline{u'_2 u'_1} & \overline{u'_2 u'_2} & \overline{u'_2 u'_3} \\ \overline{u'_3 u'_1} & \overline{u'_3 u'_2} & \overline{u'_3 u'_3} \end{pmatrix}$$

- Turbulence models with RANS
  - Equations are averages
  - But there are too few equations to the number of unknown variables (this is called Closure)
  - Therefore additional equations are needed to close the system of equations



# RANS 3

- Most well-known model to close the RANS equation is

- k- $\varepsilon$  model

- k is turbulent kinetic energy  $k = \frac{1}{2} \left( \overline{(u'_1)^2} + \overline{(u'_2)^2} + \overline{(u'_3)^2} \right)$ .
- $\varepsilon$  is the turbulent dissipation
- Are used in industrial applications

- Other models

- k- $\omega$  model
- Menter model



# RANS 4

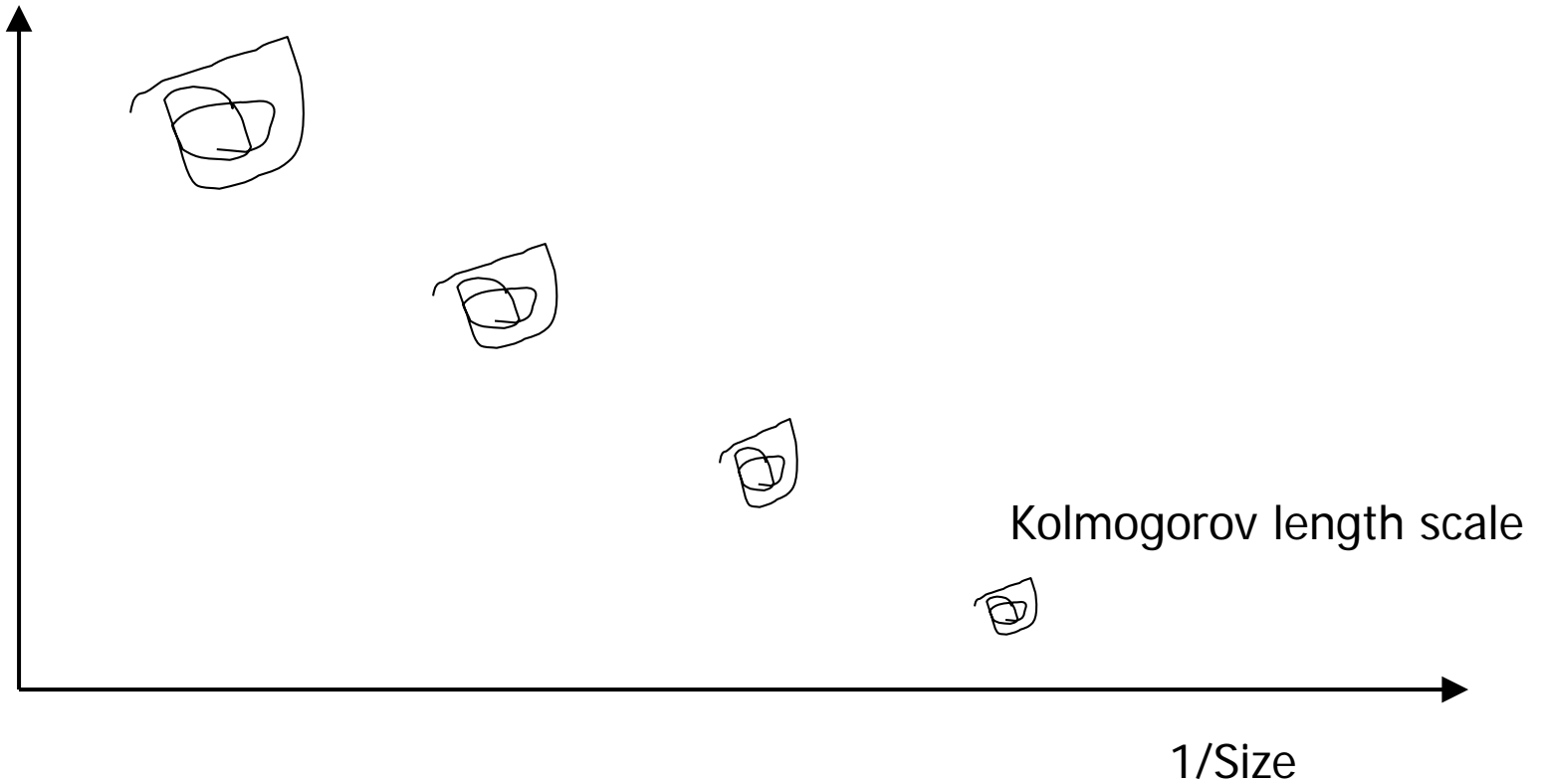
- The most time consuming closure for RANS is:
  - The Reynolds stress model
    - Gives 7 extra partial differential equations
    - Difficult to get to converge (solve)
    - It is maybe then better to use LES instead (see Versteeg, page 109)



# Turbulence cascade

Energy

Integral length scale





# LES 1

- Filtering of the equations
  - Eddies below a given size  $\Delta$  are handled by the "sub grid" model
    - $\Delta > h$  ,  $h$  is the grid size
  - Model to handle the "small" eddies, turbulent viscosity
    - Constant Smagorinsky
    - Dynamic Smagorinsky
    - Deardorff (Default in FDS 6)
    - Vreman



## LES 2

- Energy on sub-grid
  - 90 % of the eddies should be resolved in the large grid, (se Combustion af Warnatz, Maas og Dibble)
    - This is rarely the case when using FDS
    - Use Measurement of turbulent resolution





# LES 3 Turbulent viscosity

- Smagorinsky

$$\mu_t = \rho (C_s \Delta)^2 |S| \quad ; \quad |S| = \left( 2S_{ij}S_{ij} - \frac{2}{3}(\nabla \cdot \mathbf{u})^2 \right)^{\frac{1}{2}}$$

- Deardorff

$$\mu_t = \rho C_v \Delta \sqrt{k_{sgs}} \quad ; \quad k_{sgs} = \frac{1}{2} ((\bar{u} - \hat{u})^2 + (\bar{v} - \hat{v})^2 + (\bar{w} - \hat{w})^2)$$



# LES 4

## ■ Setting turbulence model in FDS

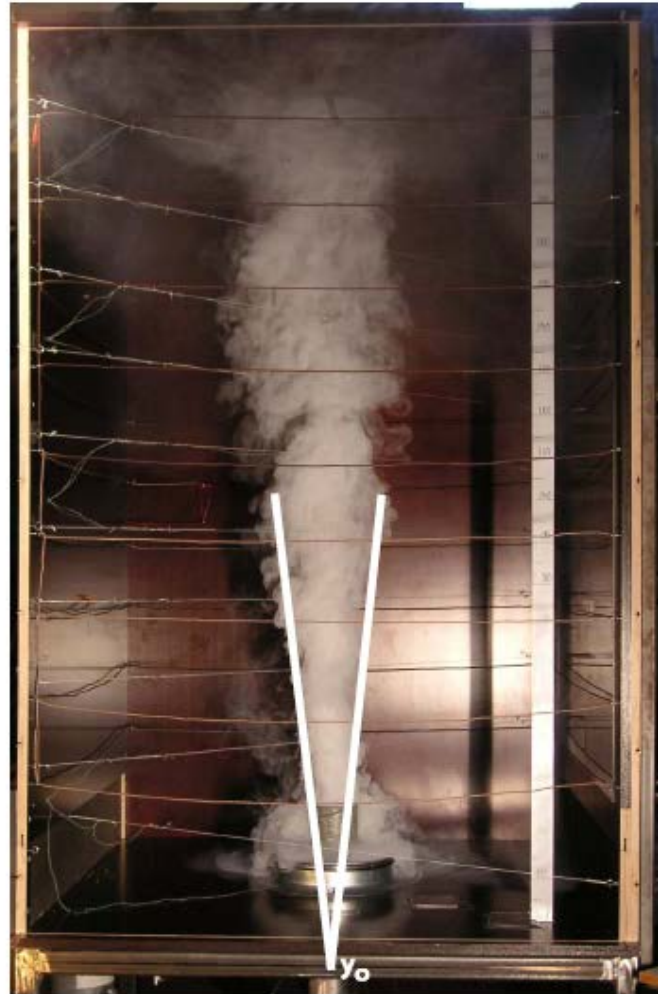
TURBULENCE_MODEL	Description	Coefficient(s)
'CONSTANT SMAGORINSKY'	Constant coefficient Smagorinsky model [11]	C_SMAGORINSKY
'DYNAMIC SMAGORINSKY'	Dynamic Smagorinsky model [12, 13]	None
'DEARDORFF'	Deardorff model [9, 10]	C_DEARDORFF
'VREMAN'	Vreman's eddy viscosity model [14]	C_VREMAN
'RNG'	Renormalization group eddy viscosity model [15]	C_RNG, C_RNG_CUTOFF



# Smagorinsky constant ( $C_s$ )

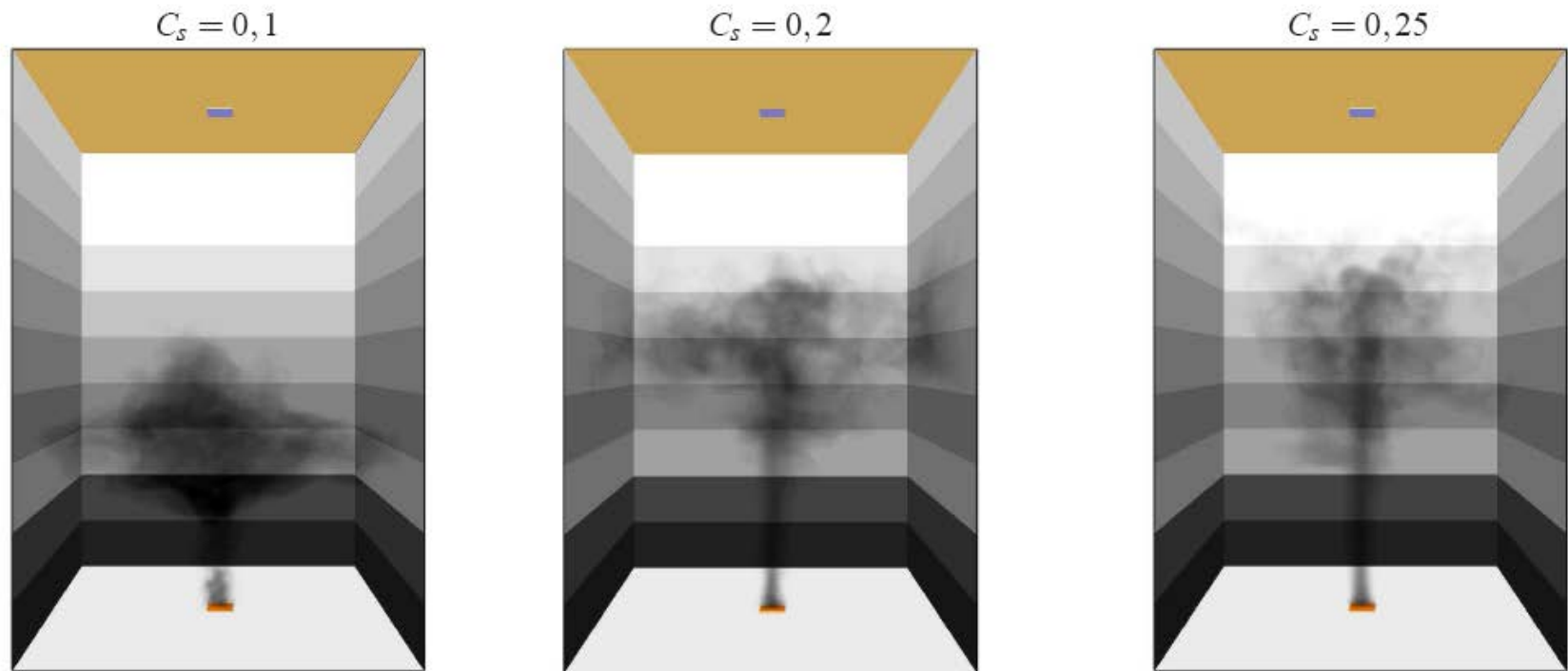
- What should it be (FDS 5)
  - It is set to 0.20, but it depends on the geometry
- Example from Sommerlund-Larsen and Petersen's, M.Sc. Thesis
- FDS 6 uses a dynamic Smagorinsky model

# Experiment – Sommerlund-Larsen and Petersen



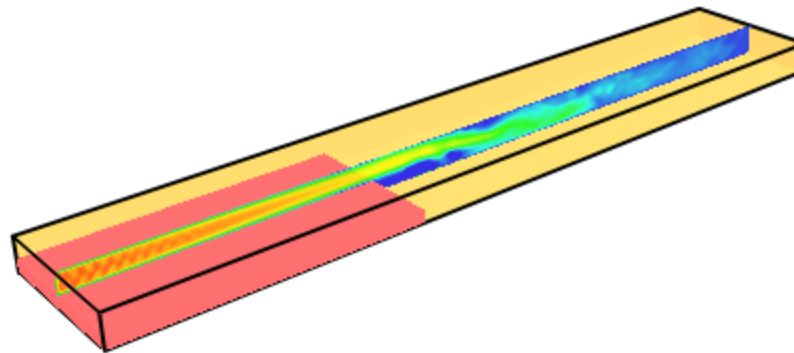
*Plumen under forsøg med opdriftsneutralt røglag, hvor spredningsvinklen er fundet til  $14^\circ$ .*

# Different value of $C_s$ (Fixed Smagorinsky constant)



**Figur M.11:** Røglagets udvikling efter 40 sekunders 14x14 cm 50 W brand. De tre brande har forskellige Smagorinsky konstanter; og fra venstre af, antager de værdierne 0,1, 0,2 og 0,25.

# Backward facing step



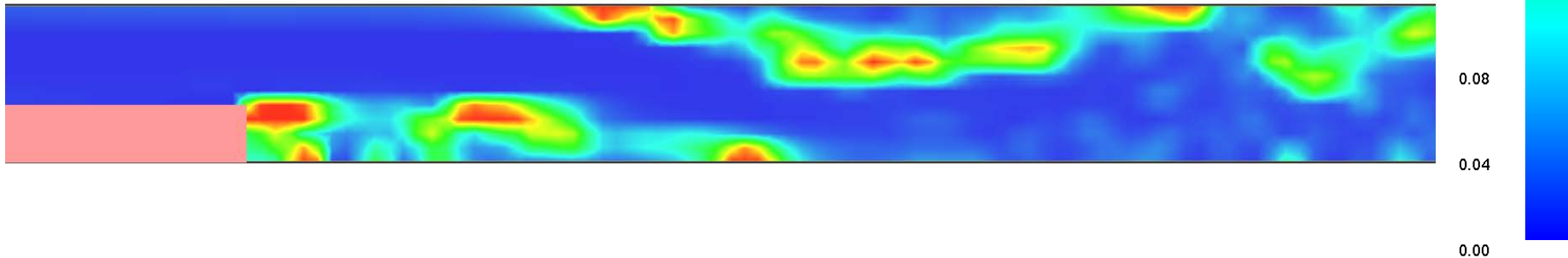
Slice  
U-VEL  
m/s  
 $\times 10^{-2}$

145  
130  
115  
100  
85.0  
70.0  
55.0  
40.0  
25.0  
10.0  
-5.00

Time: 16.18

# Dynamic Smagorinsky constant

- Backward facing step
  - Shows the amount of turbulent energy that are resolved
  - Larger blue area is better (means less energy is handled by the Smagorinsky model)



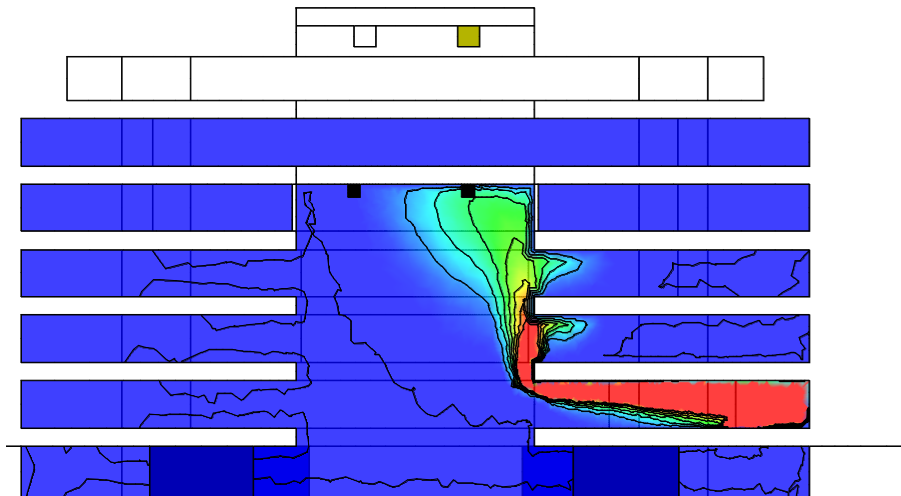
# RANS versus LES

Kontorhus med atrium

1 MW fast brand – mekanisk udsugning

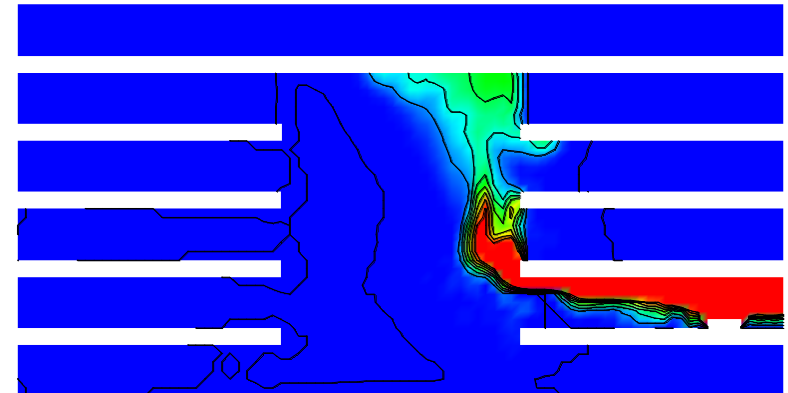
90 sekunder

RANS model



CFX 5.7

LES model



FDS 4.03

Temperatur



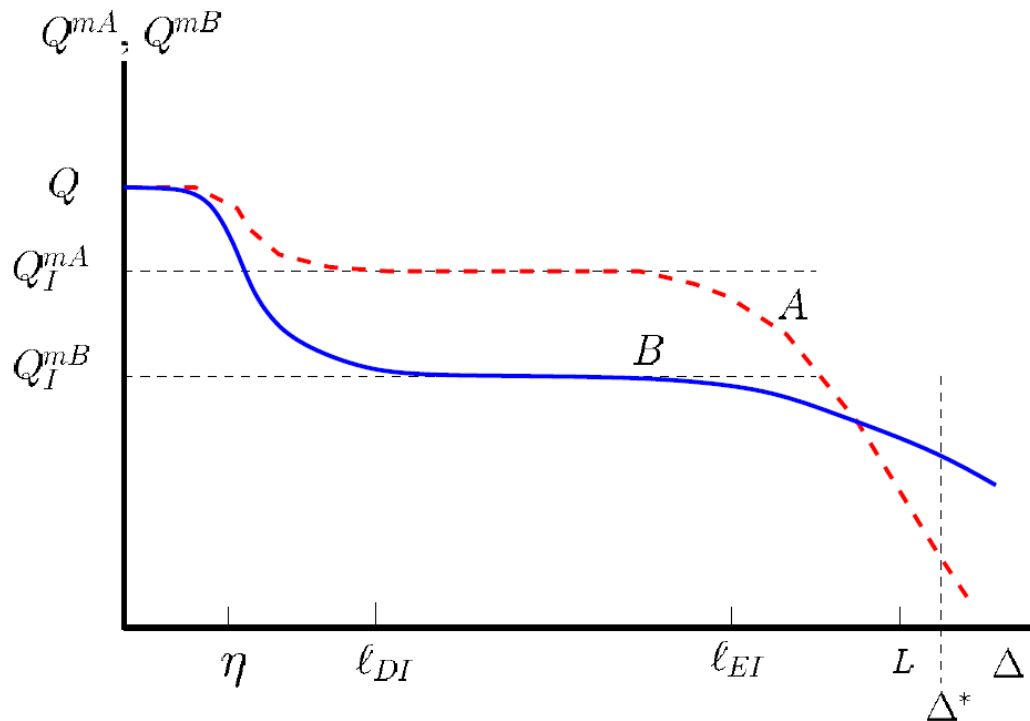




# Pope's questions

- 1. Is LES the right approach?
- 2. Can the resolution of all scales be made tractable?
- 3. Do we have sufficient computer power for LES?
- 4. Is LES a physical model, a numerical procedure or a combination of both?
- 5. How can LES be made complete? (MTR)
- 6. What is the relationship between  $U$  and  $W$ ?
- 7. How do predicted flow statistics depend on ?
- 8. What is the goal of an LES calculation?
- 9. How are different LES models to be appraised?
- 10. Why is the dynamic procedure successful?

# Statistic, question 7



**Figure 5.** The predictions  $Q^{mA}(\Delta)$  and  $Q^{mB}(\Delta)$  of the statistic  $Q$  obtained from LES models A and B as functions of the turbulence resolution length scale  $\Delta$  for the case in which  $Q$  has contributions from both energy-containing and dissipative scales.